# FEASIBILITY STUDY of the R112 (Demra Staff Quarter to Rampra) ROAD WIDENING PROJECT 

Submitted to the Faculty of East West University by

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## Executive Summary

The goal of this report is to find out if a road widening is needed or not. To find that out, level of service (LOS) is calculated in the very beginning. The LOS provides evidence as how long the current pavement can sustain and the expected lifetime of the planned widened road. As the level of service is found to be quite good for the future planned road, so the next task is to choose the type of pavement. Cost benefit analysis helps to choose the best possible pavement.

## Introduction

Dhaka is known for having the highest population density, according to a report from Statista Research Department, 2022. Traffic congestion is a common scenario in Dhaka city. To reduce the day-to-day traffic congestion, road widening and construction of new roads are inevitable. However, the budget for this sector is limited. The road construction authorities like RHD, LGED, or city corporations cannot start widening any road due to the strict budget. That is why a feasibility study is required. A feasibility study compares multiple options based on service and budget, and forecasts these for a future time period, and provides the best possible solution.

The R112 is an important highway in Dhaka city. Each lane should be at least 12 ft wide to call it a lane. Following this definition, the R112 highway is a two-lane highway. This highway connects North Dhaka to two major highways in Bangladesh. One is N1, which connects Dhaka to Chattogram. Another one is N2 which connects Dhaka to Sylhet. The R112 is the only road that connects North Dhaka to these two major national highways. Due to it, the demand for this road is increasing exponentially.

The road was able to provide free flow speed even three to four years ago. Nowadays, traffic congestion can often be seen on this road. That is why this road was chosen for this feasibility study. The feasibility study will provide evidence as to if the road width is sufficient for upcoming days and if a road widening is implemented, whether it will be beneficial.

### 1.2 Problem Statement:

The level of service of the current road and the future anticipated road after widening will provide us with evidence of whether to widen the road. There are several ways to design pavement for a road. In this project, the pavement design is broadly classified into two categories, one is rigid pavement, another one is flexible pavement. Among rigid pavement, two types of pavement design are considered. Among flexible pavement, three types of pavement design are considered. The best possible pavement design will be chosen from the cost-benefit ratio of each pavement. The cost mainly comes from the construction cost, repair and rehabilitation cost, and reconstruction cost. The benefit comes from multiple criteria. Those come from two different types of cost. One is road user cost which includes travel time cost, and vehicle operating cost. The other type is environmental impact cost which includes noise
pollution cost, vehicle emission cost, and safety cost. Comparing all these costs in terms of current condition and anticipated widening condition, the benefit can be measured. Using these costs and benefits, a ratio will be calculated to find out the best possible pavement design for this road.

### 1.3 Objectives of the Study:

- Find out the level of service for current and future anticipated road
- Geometric design to find out the visible portion of the road
- Structural design to find out the thickness of each layer of the pavement
- Cost Analaysis for each type of pavement
- Benefit Analaysis for each type of pavement
- Choosing the best possible pavement based on the cost benefit analysis


## Chapter 1

## Level of Service

This method of finding Level of Service (LOS) is applicable for highway sections of at least 2 miles ( 3.22 km ). Our road segment is 5.28 mile ( 8.508 km ). So, this method to find LOS is applicable to our road segment.

## Estimating FFS:

$\mathrm{FFS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}-\mathrm{f}_{\mathrm{A}} \quad \mathrm{Eq} 1$

EXHIBIT 20-5. ADJUSTMENT ( $\mathrm{f}_{\text {LS }}$ ) FOR LANE WIDTH AND ShOULDER WIDTH

| Lane Width (tt) | Reduction in FFS (mi/h) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Shoulder Width (t) |  |  |  |
|  | 6.4 | $\geq 2<4$ | $\geq 4<6$ | $\geq 6$ |
| $\geq 10<11$ | 5.3 | 3.8 | 3.5 | 2.2 |
| $\geq 11<12$ | 4.7 | 3.0 | 1.4 | 1.1 |
| $\geq 12$ | 4.2 | 2.6 | 1.3 | 0.4 |

One lane $=3.65 \mathrm{~m}(12 \mathrm{ft}) \geq 12 \mathrm{ft}$
Shoulder width $=2 \mathrm{ft} \geq 2<4 \mathrm{ft}$
From Exhibit 20-5, Adjustment for lane width and shoulder width, $\mathrm{f}_{\mathrm{LS}}=2.6$
EXHIBIT 20-6. ADJUSTMENT ( $\mathrm{f}_{\mathrm{A}}$ ) FOR ACCESS-POINT DENSITY

| Access Points per mi | Reduction in FFS (mi/h) |
| :---: | :---: |
| 0 | 0.0 |
| 10 | 2.5 |
| 20 | 5.0 |
| 30 | 7.5 |
| 40 | 10.0 |

Total access points $=20$
Total road length $=5.28$ mile
Access point per mile $=\frac{20}{5.28}=3.79<10$

From Exhibit 20-6, Adjustment $\mathrm{f}_{\mathrm{A}}$ for access point density $=2.5 \mathrm{mi} / \mathrm{h}$
Base FFS, BFFS $=49.71 \mathrm{mi} / \mathrm{h}(80 \mathrm{~km} / \mathrm{h})$
From Eq 1,
$\mathrm{FFS}=\mathrm{BFFS}-\mathrm{f}_{\mathrm{LS}}-\mathrm{f}_{\mathrm{A}}=49.71-2.6-2.5=44.61 \mathrm{mi} / \mathrm{h}$

## Demand Flow Rate:

Demand flow rate, $\mathrm{v}_{\mathrm{p}}=\frac{V}{P H F * f G * f H V} \quad$ Eq 2
Assuming, Peak hour factor, $\mathrm{PHF}=0.95$

EXhibit 20-7. GRADE AdJustment Factor ( $\mathrm{f}_{\mathrm{G}}$ ) to DETERMIne SPEEDS ON Two-WAY and DIRECTIONAL SEGMENTS

| Range of Two-Way Flow <br> Rates (pc/h) | Range of Directional Flow <br> Rates (pc/h) | Type of Terrain |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $0-300$ | Level | Rolling |  |
|  | $>300-600$ | 1.00 | 0.71 |  |
| $>600-1200$ | $>600$ | 1.00 | 0.93 |  |
| $>1200$ | 1.00 | 0.99 |  |  |

Passenger car per hour $=\frac{2916}{24}=121.5$ which is between 0-600
Range of directional flow $=60.75$ which is between 0-300
Terrain level $=$ Level
From Exhibit 20-7, $\mathrm{f}_{\mathrm{G}}$ to determine speeds $=1$

EXHIBIT 20-8. GRADE ADJUSTMENT FACTOR ( $\mathrm{f}_{\mathrm{G}}$ ) TO DETERMINE PERCENTTIME-SPENT-FOLLOWING ON TWO-WAY AND DIRECTIONAL SEGMENTS

| Range of Two-Way Flow <br> Rates (pc/h) | Range of Directional Flow <br> Rates (pc/h) | Type of Terrain |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $0-600$ |  | Level |  |
|  | $>300-600$ | 1.00 | Rolling |  |
| $>1200$ | $>600$ | 1.00 | 0.77 |  |

From Exhibit 20-8, $\mathrm{f}_{\mathrm{G}}$ to determine percent-time-spent-following $=1$

EXHIBIT 20-9. PASSENGER-CAR EQUIVALENTS FOR TRUCKS AND RVS TO DETERMINE SPEEDS ON TWO-WAY AND DIRECTIONAL SEGMENTS

| Vehicle Type | Range of Two-Way <br> Flow Rates (pc/h) | Range of Directional <br> Flow Rates (pc/h) | Type of Terrain |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $0-300$ | Level | Rolling |
| Trucks, $\mathrm{E}_{\mathrm{T}}$ | $>600-1,200$ | $>300-600$ | 1.7 | 2.5 |
|  | $>1,200$ | $>600$ | 1.1 | 1.9 |
|  | $0-600$ | $0-300$ | 1.0 | 1.5 |
| RVs, $\mathrm{E}_{\mathrm{R}}$ | $>600-1,200$ | $>300-600$ | 1.0 | 1.1 |
|  | $>1,200$ | $>600$ | 1.0 | 1.1 |
|  |  |  |  |  |

EXHIBIT 20-10. PASSENGER-CAR EQUIVALENTS FOR TRUCKS AND RVS TO DETERMINE PERCENT TIME-SPENT-FOLLOWING ON TWO-WAY AND DIRECTIONAL SEGMENTS

| Vehicle Type |  |  | Range of Two-Way |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Flow Rates (pc/h) |  |  |  | \(\begin{array}{c}Range of Directional <br>

\)\cline { 4 - 5 } <br>
\cline { 4 - 5 } <br>
Flow Rates (pc/h)\end{array}$)$

For Trucks (including buses),
Range of two way flow rates $=\frac{10116}{24}=421.5 \mathrm{pc} / \mathrm{h}$ within 0-600
Range of directional flow rate $=210.75 \mathrm{pc} / \mathrm{h}$ within $0-300$

Type of terrain = Level
From Exhibit 20-9, $\mathrm{E}_{\mathrm{T}}$ to determine speeds $=1.7$
For RVs (including utility),
Range of two way flow rates $=\frac{276}{24}=11.5 \mathrm{pc} / \mathrm{h}$ within 0-600
Range of directional flow rates $=5.75$ within 0-300

Type of terrain = Level
From Exhibit 20-9, $\mathrm{E}_{\mathrm{R}}$ to determine speeds $=1.0$
From Exhibit 20-10, Trucks, $\mathrm{E}_{\mathrm{T}}$ to determine percent-time-spent-following $=1.1$
From Exhibit 20-10, RVs, $\mathrm{E}_{\mathrm{R}}$ to determine percent-time-spent-following $=1.0$
Heavy vehicle adjustment factor, $\mathrm{f}_{\mathrm{HV}}=\frac{1}{1+P T(E T-1)+P R(E R-1)} \quad \mathrm{Eq} 3$
Here, proportion of trucks in the traffic stream, $\mathrm{P}_{\mathrm{T}}=\frac{10116}{17074}=0.59$
proportion of RVs in the traffic stream, $\mathrm{P}_{\mathrm{R}}=\frac{276}{17074}=0.016$

## Using Eq 3,

For determining speed, $\mathrm{f}_{\mathrm{HV}}=\frac{1}{1+0.59(1.7-1)+0.016(1-1)}=0.71$
For determining percent-time-spent-following, $\mathrm{f}_{\mathrm{HV}}=\frac{1}{1+0.59(1.1-1)+0.016(1-1)}=0.94$
Flow rate, $\mathrm{v}=\frac{17074}{24}=711.42 \mathrm{v} / \mathrm{hr}$
Demand flow rate, $\mathrm{v}_{\mathrm{p}}=\frac{V}{P H F * f G * f H V}=\frac{711.42}{0.95 \times 1 \times 0.71}=1054.74 \mathrm{veh} / \mathrm{hr}$
As the value of $v_{p}(1682.83)$ is within than the flow rate range (600-1200), so the $v_{P}$ should be used.

Two way flow rate $=0.5 \mathrm{v}_{\mathrm{P}}=0.5 \times 1054.74=527.37 \mathrm{pc} / \mathrm{h}$
Average travel speed, ATS $=\mathrm{FFS}-0.00776 \mathrm{vp}_{\mathrm{p}}-\mathrm{f}_{\mathrm{np}} \quad \mathrm{Eq} 4$
Adjustment for percentage of no-passing zones, $\mathrm{f}_{\mathrm{np}}=0$
Using Eq 4, average travel speed, ATS $=44.61-(0.00776 \times 1054.74)-0=36.43 \mathrm{mi} / \mathrm{h}$
Percent time spent following, $\mathrm{PTSF}=\mathrm{BPTSF}+\mathrm{f}_{\mathrm{d} / \mathrm{np}} \quad$ Eq 5
BPTSF $=100\left(1-\mathrm{e}^{-0.000879 \mathrm{xvp}}\right)=100\left(1-\mathrm{e}^{-0.000879 \times 1054.74}\right)=60.43$
No passing zone $0 \%$ TRAFFIC AND PERCENTAGE OF NO-PASSING ZONES ON PERCENT TIME-SPENT-FOLLOWING ON TWO-WAY SEGMENTS

| Two-Way Flow Rate, $\mathrm{v}_{\mathrm{p}}$ (pc/h) | Increase in Percent Time-Spent-Following (\%) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No-Passing Zones (\%) |  |  |  |  |  |
|  | 0 | 20 | 40 | 60 | 80 | 100 |
| Directional Split $=50 / 50$ |  |  |  |  |  |  |
| $\leq 200$ | 0.0 | 10.1 | 17.2 | 20.2 | 21.0 | 21.8 |
| 400 | 0.0 | 12.4 | 19.0 | 22.7 | 23.8 | 24.8 |
| 600 | 0.0 | 11.2 | 16.0 | 18.7 | 19.7 | 20.5 |
| 800 | 0.0 | 9.0 | 12.3 | 14.1 | 14.5 | 15.4 |
| 1400 | 0.0 | 3.6 | 5.5 | 6.7 | 7.3 | 7.9 |
| 2000 | 0.0 | 1.8 | 2.9 | 3.7 | 4.1 | 4.4 |
| 2600 | 0.0 | 1.1 | 1.6 | 2.0 | 2.3 | 2.4 |
| 3200 | 0.0 | 0.7 | 0.9 | 1.1 | 1.2 | 1.4 |

Directional Split $=50 / 50$
No passing zone $0 \%$
$\mathrm{v}_{\mathrm{P}} \geq 800, \mathrm{f}_{\mathrm{d} / \mathrm{np}}=0$

No passing zone $0 \%$
Percent time-spent-following, PTSF $=60.43+0=60.43 \%$

## Determining LOS:

EXHIBIT 20-4. LOS CRITERIA FOR TWO-LANE HIGHWAYS IN CLASS II

| LOS | Percent Time-Spent-Following |
| :---: | :---: |
| A | $\leq 40$ |
| B | $>40-55$ |
| C | $>55-70$ |
| D | $>70-85$ |
| E | $>85$ |

Percent tie spent following is almost $60.43 \%$
So, according to Exhibit 20-4, LOS is C.

|  | Parement Design Life | Traffic Groorth Rate |
| :--- | :--- | :--- |
| National Road | 20 years | $10 \% \mathrm{pa}$ |
| Regional Road | 20 years | $7 \% \mathrm{pa}$ |

## Table 2: Pavement Design Life and Traffic Groorth Rates

Following the same procedure, future level of service was determined. In the A-Table 1, the AADT forecast is shown. For the forecast, $7 \%$ traffic growth rate was considered as mentioned in the RHD pavement guide.

Table 1.1: LOS on current two lane condition

| Year | LOS |
| :--- | :--- |
| 1 | C |
| 8 | D |
| 14 | E |
| 20 | F |

A-Table 5 shows the level of service in the upcoming years. Some important years to note was provided in the figure. It showed, the level of service(LOS) will be worsen in near future. The current LOS is C. The LOS will be D in 10 years, and E in 14 years. Within 20 years, the LOS will be F .

As the LOS will get lower soon, a new road construction can be considered. For trial purpose, widening of two lane roadway was considered. Under that consideration, multilane highway procedure was followed to find out the LOS for the proposed road.

Table 1.2: LOS on expected four lane condition

| Year | LOS |
| :--- | :--- |
| 1 | A |
| 12 | B |
| 19 | C |


| 25 | D |
| :--- | :--- |
| 29 | E |
| 33 | F |

This table is a summery of A-Table 8. This table shows the important years to look at. As shown in the table, the level of service will become A if the road is widened. Having a LOS A is desirable in any road.

The level of service will become B in 12 years. LOS will become C in 19 years. As the figure 1 shows, RHD pavement design life is considered to be 20 years. After the expected design life, LOS C is excellent.

The LOS will turn to F after 33 years. The road will be able to accommodate the growing demand till 33 years. So, widening two more lane will be a good decision based on the LOS.

A-Table 1: AADT Forecast

| Year | AADT Forecast | Year | AADT Forecast |
| :--- | :--- | :--- | :--- |
| 1 | 18269.18 | 26 | 99154.74 |
| 2 | 19548.02 | 27 | 106095.6 |
| 3 | 20916.38 | 28 | 113522.3 |
| 4 | 22380.53 | 29 | 121468.8 |
| 5 | 23947.17 | 30 | 129971.6 |
| 6 | 25623.47 | 31 | 139069.7 |
| 7 | 27417.11 | 32 | 148804.5 |
| 8 | 29336.31 | 33 | 159220.9 |
| 9 | 31389.85 | 34 | 170366.3 |
| 10 | 33587.14 | 35 | 182292 |


| 11 | 35938.24 | 36 | 195052.4 |
| :--- | :--- | :--- | :--- |
| 12 | 38453.92 | 37 | 208706.1 |
| 13 | 41145.69 | 38 | 223315.5 |
| 14 | 44025.89 | 39 | 238947.6 |
| 15 | 47107.7 | 40 | 255673.9 |
| 16 | 50405.24 | 41 | 273571.1 |
| 17 | 53933.61 | 42 | 292721 |
| 18 | 57708.96 | 43 | 313211.5 |
| 19 | 61748.59 | 44 | 335136.3 |
| 20 | 66070.99 | 45 | 358595.9 |
| 21 | 70695.96 | 46 | 383697.6 |
| 22 | 75644.68 | 47 | 410556.4 |
| 23 | 80939.81 | 48 | 439295.3 |
| 24 | 86605.59 | 49 | 470046 |
| 25 | 92667.98 | 50 | 502949.2 |

A-Table 2: Truck Forecast

| Year | Truck Forecast | Year | Truck Forecast |
| :--- | :--- | :--- | :--- |
| 1 | 10824.12 | 26 | 58747.18 |
| 2 | 11581.81 | 27 | 62859.48 |
| 3 | 12392.53 | 28 | 67259.65 |
| 4 | 13260.01 | 29 | 71967.82 |
| 5 | 14188.21 | 30 | 77005.57 |
| 6 | 15181.39 | 31 | 82395.96 |
| 7 | 16244.09 | 32 | 88163.68 |
| 8 | 17381.17 | 33 | 94335.14 |
| 9 | 18597.85 | 34 | 100938.6 |
| 10 | 19899.7 | 35 | 108004.3 |
| 11 | 21292.68 | 36 | 115564.6 |
| 12 | 22783.17 | 37 | 123654.1 |
| 13 | 24377.99 | 38 | 132309.9 |


| 14 | 26084.45 | 39 | 141571.6 |
| :--- | :--- | :--- | :--- |
| 15 | 27910.36 | 40 | 151481.6 |
| 16 | 29864.09 | 41 | 162085.3 |
| 17 | 31954.57 | 42 | 173431.3 |
| 18 | 34191.39 | 43 | 185571.5 |
| 19 | 36584.79 | 44 | 198561.5 |
| 20 | 39145.73 | 45 | 212460.8 |
| 21 | 41885.93 | 46 | 227333.1 |
| 22 | 44817.94 | 47 | 243246.4 |
| 23 | 47955.2 | 48 | 260273.6 |
| 24 | 51312.06 | 49 | 278492.8 |

A-Table 3: RV Forecast

| Year | RV Forecast | Year | RV Forecast |
| :--- | :--- | :--- | :--- |
| 1 | 295.32 | 26 | 1602.829 |
| 2 | 315.9924 | 27 | 1715.027 |
| 3 | 338.1119 | 28 | 1835.079 |
| 4 | 361.7797 | 29 | 1963.535 |
| 5 | 387.1043 | 30 | 2100.982 |
| 6 | 414.2016 | 31 | 2248.051 |
| 7 | 443.1957 | 32 | 2405.415 |
| 8 | 474.2194 | 33 | 2573.794 |
| 9 | 507.4147 | 34 | 2753.959 |
| 10 | 542.9338 | 35 | 2946.736 |
| 11 | 621.6049 | 36 | 3153.008 |
| 12 | 665.1172 | 37 | 3373.719 |
| 13 | 711.6754 | 38 | 3609.879 |
| 14 | 761.4927 | 39 | 3862.57 |
| 15 | 814.7972 | 40 | 4132.95 |
| 16 | 871.833 | 41 | 4422.257 |
| 17 |  | 42 | 4731.815 |


| 18 | 932.8613 | 43 | 5063.042 |
| :--- | :--- | :--- | :--- |
| 19 | 998.1616 | 44 | 5417.455 |
| 20 | 1068.033 | 45 | 5796.677 |
| 21 | 1142.795 | 46 | 6202.444 |
| 22 | 1222.791 | 47 | 6636.615 |
| 23 | 1308.386 | 48 | 7101.178 |
| 24 | 1399.973 | 49 | 7598.261 |
| 25 | 1497.971 | 50 | 8130.139 |

A-Table 4: Estimating FFS for current condition

| Year | BFFS | fLS | fA | FFS |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 49.71 | 2.6 | 2.5 | 44.61 |
| 2 | 49.71 | 2.6 | 2.5 | 44.61 |
| 3 | 49.71 | 2.6 | 2.5 | 44.61 |
| 4 | 49.71 | 2.6 | 2.5 | 44.61 |
| 5 | 49.71 | 2.6 | 2.5 | 44.61 |
| 6 | 49.71 | 2.6 | 2.5 | 44.61 |
| 7 | 49.71 | 2.6 | 2.5 | 44.61 |
| 8 | 49.71 | 2.6 | 2.5 | 44.61 |
| 9 | 49.71 | 2.6 | 2.5 | 44.61 |
| 10 | 49.71 | 2.6 | 2.5 | 44.61 |
| 11 | 49.71 | 2.6 | 2.5 | 44.61 |
| 12 | 49.71 | 2.6 | 2.5 | 44.61 |
| 13 | 49.71 | 2.6 | 2.5 | 44.61 |
| 14 | 49.71 | 2.6 | 2.5 | 44.61 |
| 15 | 49.71 | 2.6 | 2.5 | 44.61 |
| 16 | 49.71 | 2.6 | 2.5 | 44.61 |
| 17 | 49.71 | 2.6 | 2.5 | 44.61 |
| 18 | 49.71 | 2.6 | 2.5 | 44.61 |
| 19 | 49.71 | 2.6 | 2.5 | 44.61 |
| 20 | 49.71 | 2.6 | 2.5 | 44.61 |


| 21 | 49.71 | 2.6 | 2.5 | 44.61 |
| :---: | :---: | :---: | :---: | :---: |
| 22 | 49.71 | 2.6 | 2.5 | 44.61 |
| 23 | 49.71 | 2.6 | 2.5 | 44.61 |
| 24 | 49.71 | 2.6 | 2.5 | 44.61 |
| 25 | 49.71 | 2.6 | 2.5 | 44.61 |
| 26 | 49.71 | 2.6 | 2.5 | 44.61 |
| 27 | 49.71 | 2.6 | 2.5 | 44.61 |
| 28 | 49.71 | 2.6 | 2.5 | 44.61 |
| 29 | 49.71 | 2.6 | 2.5 | 44.61 |
| 30 | 49.71 | 2.6 | 2.5 | 44.61 |
| 31 | 49.71 | 2.6 | 2.5 | 44.61 |
| 32 | 49.71 | 2.6 | 2.5 | 44.61 |
| 33 | 49.71 | 2.6 | 2.5 | 44.61 |
| 34 | 49.71 | 2.6 | 2.5 | 44.61 |
| 35 | 49.71 | 2.6 | 2.5 | 44.61 |
| 36 | 49.71 | 2.6 | 2.5 | 44.61 |
| 37 | 49.71 | 2.6 | 2.5 | 44.61 |
| 38 | 49.71 | 2.6 | 2.5 | 44.61 |
| 39 | 49.71 | 2.6 | 2.5 | 44.61 |
| 40 | 49.71 | 2.6 | 2.5 | 44.61 |
| 41 | 49.71 | 2.6 | 2.5 | 44.61 |
| 42 | 49.71 | 2.6 | 2.5 | 44.61 |
| 43 | 49.71 | 2.6 | 2.5 | 44.61 |
| 44 | 49.71 | 2.6 | 2.5 | 44.61 |
| 45 | 49.71 | 2.6 | 2.5 | 44.61 |
| 46 | 49.71 | 2.6 | 2.5 | 44.61 |
| 47 | 49.71 | 2.6 | 2.5 | 44.61 |
| 48 | 49.71 | 2.6 | 2.5 | 44.61 |
| 49 | 49.71 | 2.6 | 2.5 | 44.61 |
| 50 | 49.71 | 2.6 | 2.5 | 44.61 |

A-Table 5: Finding fHV for current condition

| PHF | Pass car/hr | fg | truck <br> two way <br> flow rate | RV two <br> way flow <br> rate | ET | ER | PT | PR | fHV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.95 | 130.005 | 1 | 451.005 | 12.305 | 1.7 | 1 | 0.59248 | 0.016165 | 0.706846 |
| 0.95 | 139.1054 | 1 | 482.5754 | 13.16635 | 1.7 | 1 | 0.59248 | 0.016165 | 0.706846 |
| 0.95 | 148.8427 | 1 | 516.3556 | 14.08799 | 1.7 | 1 | 0.59248 | 0.016165 | 0.706846 |
| 0.95 | 159.2617 | 1 | 552.5005 | 15.07415 | 1.7 | 1 | 0.59248 | 0.016165 | 0.706846 |
| 0.95 | 170.41 | 1 | 591.1756 | 16.12934 | 1.7 | 1 | 0.59248 | 0.016165 | 0.706846 |
| 0.95 | 182.3387 | 1 | 632.5578 | 17.2584 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 195.1024 | 1 | 676.8369 | 18.46649 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 208.7596 | 1 | 724.2155 | 19.75914 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 223.3728 | 1 | 774.9106 | 21.14228 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 239.0089 | 1 | 829.1543 | 22.62224 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 255.7395 | 1 | 887.1951 | 24.2058 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 273.6413 | 1 | 949.2988 | 25.9002 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 292.7962 | 1 | 1015.75 | 27.71322 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 313.2919 | 1 | 1086.852 | 29.65314 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 335.2223 | 1 | 1162.932 | 31.72886 | 1.2 | 1 | 0.59248 | 0.016165 | 0.894058 |
| 0.95 | 358.6879 | 1 | 1244.337 | 33.94988 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 383.796 | 1 | 1331.441 | 36.32637 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 410.6618 | 1 | 1424.641 | 38.86922 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 439.4081 | 1 | 1524.366 | 41.59007 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 470.1667 | 1 | 1631.072 | 44.50137 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 503.0783 | 1 | 1745.247 | 47.61647 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 538.2938 | 1 | 1867.414 | 50.94962 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 575.9744 | 1 | 1998.133 | 54.51609 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 616.2926 | 1 | 2138.003 | 58.33222 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |


| 0.95 | 659.4331 | 1 | 2287.663 | 62.41548 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.95 | 705.5934 | 1 | 2447.799 | 66.78456 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 754.9849 | 1 | 2619.145 | 71.45948 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 807.8339 | 1 | 2802.485 | 76.46164 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 864.3822 | 1 | 2998.659 | 81.81396 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 924.889 | 1 | 3208.566 | 87.54093 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 989.6312 | 1 | 3433.165 | 93.6688 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1058.905 | 1 | 3673.487 | 100.2256 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1133.029 | 1 | 3930.631 | 107.2414 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1212.341 | 1 | 4205.775 | 114.7483 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1297.205 | 1 | 4500.179 | 122.7807 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1388.009 | 1 | 4815.192 | 131.3753 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1485.17 | 1 | 5152.255 | 140.5716 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1589.131 | 1 | 5512.913 | 150.4116 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1700.371 | 1 | 5898.817 | 160.9404 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1819.397 | 1 | 6311.734 | 172.2063 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 1946.754 | 1 | 6753.555 | 184.2607 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2083.027 | 1 | 7226.304 | 197.159 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2228.839 | 1 | 7732.146 | 210.9601 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2384.858 | 1 | 8273.396 | 225.7273 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2551.798 | 1 | 8852.533 | 241.5282 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2730.424 | 1 | 9472.211 | 258.4352 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 2921.553 | 1 | 10135.27 | 276.5256 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 3126.062 | 1 | 10844.73 | 295.8824 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 3344.886 | 1 | 11603.87 | 316.5942 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |
| 0.95 | 3579.029 | 1 | 12416.14 | 338.7558 | 1.1 | 1 | 0.59248 | 0.016165 | 0.944066 |

A-Table 6: Finding Level of service (LOS) for current condition

| Year | v | vp | ATS | PTSF |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 761.2158 | 1133.599 | 35.81327 | 63.08063 | C |
| 2 | 814.5009 | 1212.951 | 35.1975 | 65.56801 | C |


| 3 | 871.516 | 1297.858 | 34.53862 | 68.04422 | C |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 4 | 932.5221 | 1388.708 | 33.83363 | 70.49688 | C |
| 5 | 997.7987 | 1485.917 | 33.07928 | 72.91314 | C |
| 6 | 1067.645 | 1257.006 | 34.85563 | 66.87589 | C |
| 7 | 1142.38 | 1344.997 | 34.17282 | 69.34126 | C |
| 8 | 1222.346 | 1439.147 | 33.44222 | 71.77635 | D |
| 9 | 1307.911 | 1539.887 | 32.66048 | 74.16812 | D |
| 10 | 1399.464 | 1647.679 | 31.82401 | 76.50329 | D |
| 11 | 1497.427 | 1763.017 | 30.92899 | 78.76866 | D |
| 12 | 1602.247 | 1886.428 | 29.97132 | 80.95127 | D |
| 13 | 1714.404 | 2018.478 | 28.94661 | 83.0388 | D |
| 14 | 1834.412 | 2159.771 | 27.85018 | 85.01977 | E |
| 15 | 1962.821 | 2310.955 | 26.67699 | 86.8839 | E |
| 16 | 2100.218 | 2341.739 | 26.4381 | 87.23405 | E |
| 17 | 2247.234 | 2505.661 | 25.16607 | 88.94708 | E |
| 18 | 2404.54 | 2681.057 | 23.805 | 90.52629 | E |
| 19 | 2572.858 | 2868.731 | 22.34865 | 91.96702 | E |
| 20 | 2752.958 | 3069.542 | 20.79035 | 93.26685 | F |

A-Table 7: FFS for proposed multilane highway

| Year | BFFS | fLW | fLC | fM | fA | FFS |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 2 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 3 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 4 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 5 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 6 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 7 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 8 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 9 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 10 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |


| 11 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 13 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 14 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 15 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 16 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 17 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 18 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 19 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 20 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 21 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 22 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 23 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 24 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 25 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 26 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 27 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 28 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 29 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 30 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 31 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 32 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 33 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 34 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 35 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 36 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 37 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 38 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 39 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 40 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |


| 41 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 42 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 43 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 44 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 45 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 46 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 47 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 48 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 49 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |
| 50 | 49.71 | 0 | 1.8 | 0 | 0 | 47.91 |

A-Table 8: Estimating Vp for proposed multilane highway

| TLC | V | PHF | N | fHV | fp | vp |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.8 | 761.2158 | 0.95 | 4 | 0.769543 | 1 | 260.3104 |
| 1.8 | 814.5009 | 0.95 | 4 | 0.769543 | 1 | 278.5321 |
| 1.8 | 871.516 | 0.95 | 4 | 0.769543 | 1 | 298.0293 |
| 1.8 | 932.5221 | 0.95 | 4 | 0.769543 | 1 | 318.8914 |
| 1.8 | 997.7987 | 0.95 | 4 | 0.769543 | 1 | 341.2138 |
| 1.8 | 1067.645 | 0.95 | 4 | 0.769543 | 1 | 365.0987 |
| 1.8 | 1142.38 | 0.95 | 4 | 0.769543 | 1 | 390.6556 |
| 1.8 | 1222.346 | 0.95 | 4 | 0.769543 | 1 | 418.0015 |
| 1.8 | 1307.911 | 0.95 | 4 | 0.769543 | 1 | 447.2616 |
| 1.8 | 1399.464 | 0.95 | 4 | 0.769543 | 1 | 478.57 |
| 1.8 | 1497.427 | 0.95 | 4 | 0.769543 | 1 | 512.0699 |
| 1.8 | 1602.247 | 0.95 | 4 | 0.769543 | 1 | 547.9148 |
| 1.8 | 1714.404 | 0.95 | 4 | 0.769543 | 1 | 586.2688 |
| 1.8 | 1834.412 | 0.95 | 4 | 0.769543 | 1 | 627.3076 |
| 1.8 | 1962.821 | 0.95 | 4 | 0.769543 | 1 | 671.2191 |
| 1.8 | 2100.218 | 0.95 | 4 | 0.769543 | 1 | 718.2045 |
| 1.8 | 2247.234 | 0.95 | 4 | 0.769543 | 1 | 768.4788 |
| 1.8 | 2404.54 | 0.95 | 4 | 0.769543 | 1 | 822.2723 |


| 1.8 | 2572.858 | 0.95 | 4 | 0.769543 | 1 | 879.8314 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.8 | 2752.958 | 0.95 | 4 | 0.769543 | 1 | 941.4196 |
| 1.8 | 2945.665 | 0.95 | 4 | 0.769543 | 1 | 1007.319 |
| 1.8 | 3151.862 | 0.95 | 4 | 0.769543 | 1 | 1077.831 |
| 1.8 | 3372.492 | 0.95 | 4 | 0.769543 | 1 | 1153.279 |
| 1.8 | 3608.566 | 0.95 | 4 | 0.769543 | 1 | 1234.009 |
| 1.8 | 3861.166 | 0.95 | 4 | 0.769543 | 1 | 1320.39 |
| 1.8 | 4131.448 | 0.95 | 4 | 0.769543 | 1 | 1412.817 |
| 1.8 | 4420.649 | 0.95 | 4 | 0.769543 | 1 | 1511.714 |
| 1.8 | 4730.094 | 0.95 | 4 | 0.769543 | 1 | 1617.534 |
| 1.8 | 5061.201 | 0.95 | 4 | 0.769543 | 1 | 1730.761 |
| 1.8 | 5415.485 | 0.95 | 4 | 0.769543 | 1 | 1851.915 |
| 1.8 | 5794.569 | 0.95 | 4 | 0.769543 | 1 | 1981.549 |
| 1.8 | 6200.189 | 0.95 | 4 | 0.769543 | 1 | 2120.257 |
| 1.8 | 6634.202 | 0.95 | 4 | 0.769543 | 1 | 2268.675 |
| 1.8 | 7098.596 | 0.95 | 4 | 0.769543 | 1 | 2427.482 |
| 1.8 | 7595.498 | 0.95 | 4 | 0.769543 | 1 | 2597.406 |
| 1.8 | 8127.183 | 0.95 | 4 | 0.769543 | 1 | 2779.225 |
| 1.8 | 8696.086 | 0.95 | 4 | 0.769543 | 1 | 2973.77 |
| 1.8 | 9304.812 | 0.95 | 4 | 0.769543 | 1 | 3181.934 |
| 1.8 | 9956.148 | 0.95 | 4 | 0.769543 | 1 | 3404.67 |
| 1.8 | 10653.08 | 0.95 | 4 | 0.769543 | 1 | 3642.997 |
| 1.8 | 11398.79 | 0.95 | 4 | 0.769543 | 1 | 3898.006 |
| 1.8 | 12196.71 | 0.95 | 4 | 0.769543 | 1 | 4170.867 |
| 1.8 | 13050.48 | 0.95 | 4 | 0.769543 | 1 | 4462.827 |
| 1.8 | 13964.01 | 0.95 | 4 | 0.769543 | 1 | 4775.225 |
| 1.8 | 14941.49 | 0.95 | 4 | 0.769543 | 1 | 5109.491 |
| 1.8 | 15987.4 | 0.95 | 4 | 0.769543 | 1 | 5467.156 |
| 1.8 | 17106.52 | 0.95 | 4 | 0.769543 | 1 | 5849.856 |
| 1.8 | 18303.97 | 0.95 | 4 | 0.769543 | 1 | 6259.346 |


| 1.8 | 19585.25 | 0.95 | 4 | 0.769543 | 1 | 6697.501 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.8 | 20956.22 | 0.95 | 4 | 0.769543 | 1 | 7166.326 |

A-Table 9: Estimating Level of Service for proposed multilane highway

| Year | ET | ER | PT | PR | fHV | D |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 5.43332 | A |
| 2 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 5.813652 | A |
| 3 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 6.220608 | A |
| 4 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 6.65605 | A |
| 5 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 7.121974 | A |
| 6 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 7.620512 | A |
| 7 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 8.153948 | A |
| 8 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 8.724724 | A |
| 9 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 9.335455 | A |
| 10 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 9.988937 | A |
| 11 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 10.68816 | A |
| 12 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 11.43633 | B |
| 13 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 12.23688 | B |
| 14 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 13.09346 | B |
| 15 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 14.01 | B |
| 16 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 14.9907 | B |
| 17 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 16.04005 | B |
| 18 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 17.16285 | B |
| 19 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 18.36425 | C |
| 20 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 19.64975 | C |
| 21 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 21.02523 | C |
| 22 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 22.497 | C |
| 23 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 24.07179 | C |
| 24 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 25.75681 | C |
| 25 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 27.55979 | D |
| 26 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 29.48898 | D |


| 27 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 31.55321 | D |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 28 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 33.76193 | D |
| 29 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 36.12527 | E |
| 30 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 38.65403 | E |
| 31 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 41.35982 | E |
| 32 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 44.255 | E |
| 33 | 1.5 | 1.2 | 0.59248 | 0.016165 | 0.769543 | 47.35285 | F |

## Chapter 2

## Geometric Design

Type 1: 11 m wide dual - This is a three-lane carriageway as one half of a dual 3 - lane road.
Type 2: 7.3 m wide dual - This is a high standard carriageway as one half of a dual 2-lane road.
Type 3: 7.3 m wide single - This is a high standard two-lane single carriageway.
Type 4: 6.2 m wide -

Type 5: 5.5 m wide -

Type 6: 3.7 m wide -
This is the lowest economic cost option for a very wide range of traffic volumes. It allows most vehicles to pass with sufficient clearance to avoid the need to slow down or move aside.

According to RHD Geometric design manual, type 3 is a high standard two-lane single carriageway option. As the space available to widen the lanes are limited. The environmental impact was aimed to keep at a minimum. So, this type of road was chosen for the feasibility study.

Design type 3-7.3 m wide carriageway width of sectional element

Table 2.2 Typical Design Speeds

| Design <br> Type | Design Speed (km/h) |  |  |
| :---: | :---: | :---: | :---: |
|  | Plain | Rolling | Hilly |
| $1-2$ | $80-100$ | 80 | - |
| $(3)$ | 80 | 65 | 50 |
| 4 | 65 | 50 | 40 |
| $5-6$ | 50 | 40 | 30 |

According to table 2.2, design type level 3 and plain terrain should have $80 \mathrm{~km} / \mathrm{hr}$ velocity. So, this speed limit was chosen for this study.

Trucks are usually 4 m high. However, there can be transports of abnormal loads crossing this road. So, a vertical clearance of 5.7 m headroom was chosen. This headroom was ensured throughout the length of the road.

Lateral clearance is suggested to be 1 meter in the RHD manual. As there are only waterbody on the side of the road, so lateral clearance is available. Tree plantation was chosen throughout the length of road. However, trees will not be provided in places where there are horizontal curves. According to RHD manual, standard cross-fall of $3 \%$ was chosen for the curved carriageways. The RHD manual suggests to place the road pavement 1m above the flood level. However, the goal of this extended lanes is to work adjacently to the existing two lanes. So, the flood level calculation is excluded for now. The existing road was built only 9 years ago. So, the same elevation of the extended lanes is considered to be adequate.


According to the AADT data, only $0.5 \%$ of the vehicles are non-motorized. So, additional nonmotorized lane (NMT) was not provided.

Design Type 3-7.3 M Wide Carriageway without NMT Lane


Crest $=16.3 \mathrm{~m}$
Carriageway $=7.3 \mathrm{~m}$
Shoulder paved $=1.5 \mathrm{~m}$

Verge $=3.0 \mathrm{~m}$

Design capacity
Maximum capacity: 2100PCU/hr
Assumed NMT/MV ratio $=0.005$
Assuming PCE values for,
bicycle $=0.5$
Rickshaw $=2$
Car $=4$

NMT $=(17 \times 0.5)+(70 \times 2)+(4 \times 0)$

$$
=148.5 \mathrm{PCU} / \mathrm{hr}
$$

## As NMT 148.5 PCU/hr < 400 PCU/hr

So separate NMT is not required

## Horizontal Curves:

Table 5.1 Minimum Curve Radii (meters)

| Design <br> Speed <br> $\mathbf{( k m / h})$ | Single Lane <br> Roads (3.7m <br> carriageway | Two Lane Single <br> Carriageway Roads <br> $(6.2$ and 7.3m carriageway) |  | Dual Carriageway <br> Roads (2 x 7.3) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ISD | SSD $^{\text {I }}$ | ISD | OSD | ISD |
| 30 | 120 | 35 | 120 | 500 | - |
| 40 | 250 | 65 | 250 | 1000 | - |
| $50-$ | 500 | 120 | 500 | 2000 | 500 |
| 65 | 1000 | $(5250))$ | 1000 | 4000 | 1000 |
| 80 | - | $(500)$ | 2000 | 8000 | 2000 |
| 100 | - | 1000 | 4000 | - | 4000 |

According to table 5.1
Assume design speed $=80 \mathrm{~km} / \mathrm{h}$
For two lane - single carriageway roads 6.2 an
$\mathrm{SSD}=500$

ISD $=2000$

OSD $=8000$

Curves were selected according to SSD as such curves are clearly non-overtaken. So, finalized curve radii is 500 m .

Table 5.2 Minimum Super-elevation Requirements (\%)

| Design Speed (km/h) | Sight Distance (m) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
|  | 25 | 30 | 45 | 60 | 90 | (120) | 180 | 250 | 360 |
|  | Curve Radii (m)' |  |  |  |  |  |  |  |  |
|  | 20 | 35 | 65 | 120 | 250 | 500 - | 1000 | 2000 | 4000 |
|  | Minimum Super-elevation Requirement (\%) |  |  |  |  |  |  |  |  |
| 30 | 7 | 5 | 3 | Nil | Nil | - | - | - | -- |
| 40 | - | 7 | 5 | 3 | Nil | Nil | - | - | - |
| 50 | - | - | 7 | 5 | 3 | ${ }^{\mathrm{Nil}}$ | Nil | - | - |
| 65 | - | - | - | 7 | (5) | 3. | Nil. | Nil | - |
| (80): | - | - | - | - | 7. | (5) | (3) | ${ }_{-N i l}$ | Nil |
| 100 | - | - | - | - | - | 7 | 3 | 3 | Nil |

According to table 5.2,
For curve radii 500 m
Design speed $=80 \mathrm{~km} / \mathrm{hr}$
Minimum Super elevation requirement $=5 \%$

## Table 5.3 Minimum Design Transition Length (m)

| Design Speed (km/h) | Super-elevation e |  |  | Straight <br> Transition <br> Length (m) Lc |
| :---: | :---: | :---: | :---: | :---: |
|  | 7\% | 5\% | 3\% |  |
|  | Plan Transition Length (m) Lp |  |  |  |
| 30 | 25 | 15 | 10 | 10 |
| 40 | 35 | 20 | 13 | 13 |
| 50 | 45 [55] | 25 [35] | 15 [20] | 15 [20] |
| 65 | 55 [65] | 35 [45] | $\checkmark 20$ [25] | 20 [25] |
| 80 | 65 [75] | 45 [55] | $\checkmark 25$ [35] | 25 [35] |
| 100 | 75 [95] | 55 [65] | 35 [45] | 35 [45] |

## Notes:

1. Values in brackets refer to dual carriageway roads..
2. Figure 5.1 illustrates the two types of transition Lp and Lc
3. To allow scope for future road upgrades and higher design speeds it is desirable to select Lp values for one design speed and one ' $e$ ' value larger than the values given by input.

Source: : adapted from Table 7.58 and 7.59, RMSS, Vol. V11a

From table 5.3,
For Design speed $80 \mathrm{~km} / \mathrm{hr}$ and super elevation $5 \%$,

Plan transition length, $\mathrm{Lp}=45 \mathrm{~m}$

Straight transition length, Lc $=55 \mathrm{~m}$


| Radius (m) | Single Lane <br> Roads |  | Two Lane Roads |  |
| :--- | :--- | :--- | :--- | :---: |
|  | $\mathbf{3 . 7 m}$ wide | $\mathbf{6 . 2 m}$ wide | $\mathbf{7 . 3 m}$ wide- |  |
| 15 | 1.8 | 2.4 | 2.1 |  |
| 16 to 20 | 1.5 | 2.1 | 1.8 |  |
| 21 to 35 | 1.2 | 1.8 | 1.5 |  |
| 36 to 65 | 0.9 | 1.5 | 1.2 |  |
| 66 to 120 . | 0.6 | 1.2 | 0.9 |  |
| 121 to 200 | Nil | 0.9 | 0.6 |  |
| 201 to 350 | Nil | 0.6 | Nil |  |
| 351 to 600 | Nil | 0.6 | Nil |  |
| 601 to 1000 | Nil | Nil | Nil |  |

```
Notes:
1 For transitioned curves half the widening_ is applied on each side of the centerline, and it is developed uniformly over the. length of the transitions curve.
2 For curves without transitions the widening is applied on the inside of the curve, and it is developed uniformly over a 20 m length leading up to the start of the circular curve--Values in brackets refer to dual carriageway roads
```

Source: : adapted from Table 7.56, Vol. V1la, RMSS

Table 5.4

Extra carriageway width on curves for 500 m radius and 7.3 m wide two lane road is $=$ Nil.

So, no extra carriageway width on curve is required.

## Vertical curves

Parabolic vertical curve, K= L/A

Here,
$\mathrm{K}=$ length required for a $1 \%$ change of grade
$\mathrm{L}=$ length of vertical curve
$\mathrm{A}=$ change of grade in $\%$

| Design Speed (km/h) | Single Lane Roads (3.7m carriageway) | Two Lane Single Carriageway Roads <br> ( 6.2 and 7.3 m carriageway) |  |  | Dual Carriageway Roads ( $2 \times 7.3$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ISD | SSD | ISD | OSD | ISD |
| 30 | 4 | 2 | 4 | 18 | - |
| 40 | 9 | 4 | /9) | 35 | - |
| 50 | 18 | (9) | 18.) | 70 | 18 |
| -65 | 35 | (18) | (35) | 140 | (35) |
| 880 | - | (35) $/$ | 70) | 270 | 70. |
| 100 | - | 70 | 140 | 540 | 140 |

From table 6.1
For design speed $80 \mathrm{~km} / \mathrm{h}$
$\mathrm{K}=35$ for SSD

| Design <br> Speed <br> $(\mathbf{k m} / \mathbf{h})$ | Maximum Change of <br> Grade Permitted <br> Without Use of a <br> Vertical Curve | Minimum Length of <br> Vertical Curve for <br> Good Appearance <br> $(\mathbf{m})$ |
| :---: | :---: | :---: |
| 30 | 1.5 | 15 |
| 40 | 1.2 | 20 |
| 50 | 1.0 | 10 |
| 65 | 0.8 | $(40)$ |
| 80 | 0.6 | 50. |
| 100 | 0.5 | 60 |

From table 6.2 Vertical Curve Appearance Criteria
Let, $\mathrm{A} 1=5 \%$
$A 2=-5 \%$
$\therefore \mathrm{A}=5 \%-(-5 \%)=10 \%$
$\mathrm{L}=35 \times 10=350 \mathrm{~m}>50 \mathrm{~m}$

From table 6.2, L is acceptable
A curve length of 350 m is selected

Table 6.3 Maximum Gradients

| Design <br> Type | Design <br> Speed | Maximum Gradient \% |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  | Plain | Rolling | Hilly |
| All D Design <br> Type | All Design <br> Speeds | $0-3$ | $1-5$ | $(1-7)$ |

From table 6.3, gradients plain for all design type and speed, maximum gradient in plain terrain should be $=0-3 \%$

## Stopping sight distance

$\operatorname{tr}=2.5 \mathrm{~s}$
$\mathrm{V}=80$

Reaction distance, $\mathrm{dr}=0.278 \times 80=22.24 \mathrm{~m}$
$\mathrm{a}=3.4 \mathrm{~m} / \mathrm{s} 2$
$\mathrm{V}=80 \mathrm{~km} / \mathrm{h}$

Braking distance, $\mathrm{dv}=0.039 \times\left(30^{\wedge} 2 / 3.4\right)=10.32 \mathrm{~m}$
$\therefore$ Stopping slight distance $=(20.85+10.32)=31.17 \mathrm{~m}$

Stopping distance on grades,
$\mathrm{d}=0.278 . \mathrm{t} . \mathrm{v}+\left\{\mathrm{v}^{\wedge} 2 / 254(\mathrm{a} / 9.81+-\mathrm{h})\right\}$
$=(0.278 \times 2.5 \times 30)+\left\{(30)^{\wedge} 2 / 254(3.4 / 9.81+-3 / 10)\right\}$
$=30.26$ (for downgrade) And , 32.04. ( for upgrade)
$\approx 31 \mathrm{~m}$ (for downgrade)
$\approx 33 \mathrm{~m}$ ( for upgrade)

Horizontal Alignment:
Max side friction, $\mathrm{f}=\left(\mathrm{v}^{\wedge} 2 / 127 \mathrm{R}\right)$ - $\mathrm{e} / 100$

$$
\begin{aligned}
& =\left(30^{\wedge} 2 / 127 \times 35\right)-6 / 100 \\
& =0.14
\end{aligned}
$$

## Determination of Curve radius:

The radius of curvature, $R$, is the reciprocal of the curvature.
Curve radius $=\frac{a^{2}+h^{2}}{2 h}$

Now for radius of curvature R1 $=\frac{1077.78^{2}+213.24^{2}}{2 * 213.24}=2830.34 \mathrm{~m}$

Where, L1 $=2155.56$

$$
\begin{aligned}
\mathrm{H} 1 & =213.24 \\
\mathrm{~A} 1 & =\mathrm{L} 1 / 2
\end{aligned}
$$



Fig 2.1 : Location of curvature 1
For radius of curvature $\mathrm{R} 2=\frac{1591^{2}+556^{2}}{2 * 556}=2554.33 \mathrm{~m}$
Where, L2 = 3182

$$
\begin{aligned}
& \mathrm{H} 2=556 \\
& \mathrm{~A} 2=\mathrm{L} 2 / 2
\end{aligned}
$$



Fig 2.2 : Location of curvature 2

For radius of curvature $3=\frac{1636^{2}+346^{2}}{2 * 346}=4041 \mathrm{~m}$
Where, L3 $=3272$

$$
\begin{aligned}
& \mathrm{H} 3=346 \\
& \mathrm{~A} 3=\mathrm{L} 2 / 2
\end{aligned}
$$



Fig 2.3: radius of curvature 3


Fig 2.4 : total radius of curvature taken

Super-elevation : The rise given to the outer edge of a road on curves is known as super elevation. When a vehicle passes over a curved path centrifugal force acts on the vehicle. The centrifugal force tends to push the vehicle off the road. It is resisted by the friction between the tires and the road. If the frictional force is not sufficient the vehicle skids sideways. To avoid this outer edge of the road at the horizontal curve rose above the inner edge.

## Why Super-elevation is needed?

- Super elevation on curves helps keep vehicles on the road.
- Super elevation increases the stability of the fast moving vehicles on horizontal curves.
- Super elevation reduces the accidents in curves (skidding, toppling).
- On super elevated curves the vehicles need not necessarily to slow down.

FORCES ASSOCIATED WITH SUPERELEVATIDN



Fig 2.5 : Super-elevation

## Super-elevation Calculation :

$H=\frac{B v^{2}}{g R}$


Where
$\mathrm{V}=$ speed of vehicle $=80 \mathrm{~km} / \mathrm{hr}=22.22 \mathrm{~m} / \mathrm{s}$
$\mathrm{R}=$ Radius of curvature
$\mathrm{g}=$ Acceleration $=9.8 \mathrm{~m} / \mathrm{s}^{2}$
$B=$ Breath of the road

For R1,

$$
\mathrm{H} 1=\frac{7.3 * 22.22^{2}}{9.8 * 2830.34}=0.13 \mathrm{~m}
$$

For R2,

$$
\mathrm{H} 2=\frac{7.3 * 22.22^{2}}{9.8 * 2554.33}=0.14 \mathrm{~m}
$$

For R3,

$$
\mathrm{H} 3=\frac{7.3 * 22.22^{2}}{9.8 * 4041}=0.1 \mathrm{~m}
$$



Fig 2.6: Warrant for Super-elevation
From the above calculation of curve we can say that we need to provide super-elevation in our road construction.

Extra widening :Extra widening refers to the additional width of carriageway that is required on a curved section of a road over and above that required on a straight alignment.

## When necessary?

In general extra width is provided on the horizontal curves when the radius is less than 300 m .
From calculation we can say that our radius of curvature value is greater than 300 m for that we don't need to provide extra width


Fig 2.7: Study Area

Traffic Sign: Technical guidance on the design, application, location and production of traffic signs in Bangladesh is offered in the Traffic Signs Manual. Any object, gadget, line, or mark on the road that serves to convey limitations, warnings, or other information to road users or a certain class of road users is referred to as a "traffic sign." any kind of restrictions, alerts, or information. Consequently, the phrase "traffic sign" covers not only signs on posts, but also traffic lights, road studs, delineators, road markings, and other traffic management tools.

## General Principles of Traffic Signs:

Each traffic sign must fulfill the following criteria in order to be effective:

- Satisfy a demand;
- Command attention;
- Be legible;
- Express a simple, clear meaning at a glance;

Be positioned to allow for adequate response time from drivers;

- Command respect.

Signs must only be utilized when absolutely necessary. Drivers get annoyed when signs are used incorrectly or unnecessarily, and when this happens repeatedly, drivers lose respect for the sign and it loses its effectiveness when it is actually needed.

Use of traffic sign in our study area :
From the map we can see there is a hospital where we can use the sign "NO USE OF HORN"


Description: The use of vehicle horns is forbidden, as shown by this circular sign with a red diagonal running from top left to bottom right over a representation of a horn.

Application: This sign is placed outside hospitals and other places where cars are forbidden to honk their horns.

Location: The sign should be posted on the left side of the road at the start of the restriction and again after each significant intersection.
We can also use the sign of "Hospital" which is information sign C9.
COLOURS:

Background : | BLUE |
| :--- |
| with WHITE inset |

Symbol : | BLACK |
| :--- |
| with RED crescent |



## Description:

Square sign with a bed symbol, a red crescent above, and an optional panel The distance to the hospital is indicated below with an arrow or text, respectively.

Application: This sign directs drivers to a hospital's location.

Location: The sign should be placed next to the hospital and on the same side of the street. Another sign we can provide on this road is "BUS STOP" which is information sign C21.


## DESCRIPTION:

A rectangular sign with a bus icon heading left.
Application: This sign is placed to show where a bus stop is located. The sign is especially helpful at bus bays because it deters other drivers from parking there in addition to showing passengers where the bus stop is.
Location: Normally, the sign should be put up near where the buses stop.
Where a bus bay exists, though, it may be situated at the beginning of the bay.
As there is a Bazar in that road for that there should be a speed limit in that particular place which can be defined as "Special Speed Limit" which is in Regulatory Sign No A26
COLOURS:

Background : WHITE
Border : RED
Number : BLACK


## Description:

Circular sign with numbers indicating the speed limit.

## APPLICATION:

The maximum speed that is permitted on this road is given by this traffic sign.

## LOCATION:

The sign should be positioned on both sides of the road, for maximum impact. The sign should be repeated after every major junction and about every 400 meters between junctions.

These are the traffic signs we can use in our study area.

## Chapter 3

## Structural Design

### 3.1 Design analysis for flexible pavement

Flexible pavements are ashphalt making roads where asphalt make roads less susceptible to damage to bends or deflects of roads due to traffic load and it require fewer repairs over time. A flexible pavement structure is composed of several layers of different materials which together enable the road to accommodate this flexing.


Figure: layers of flexible pavement
Sub soil: sub soil or sub grade mainly consist of natural elements like sand. This part needs proper treatment so that road gets proper strength.

Aggregate base: aggregate base or subgrade base consist of stone. It is upper part of sub soil part.
Asphalt base layer: this part consist of granular materials like sand, crushed or uncrushed gravel and crushed or uncrushed slag.

Surface course: this part is the most upper part of a flexible pavement. This part consist of asphalt.

### 3.1.1 Design of flexible pavement based on RHD manual:

## California Bearing Ratio (CBR):

It's measured as the strength of the subgrade of the road. The strength of every layer is expressed as CBR for that proper material should be used and also compaction is needed to get the expected CBR value for every layer.

Table 3.1: Pavement Design life and traffic Growth rate

|  | Pavement Design Life | Traffic Growth rate |
| :--- | :--- | :--- |
| National Road | 20 years | $10 \% \mathrm{pa}$ |
| Regional Road | 20 years | $7 \% \mathrm{pa}$ |

## Determining Cumulative ESAs over the Pavement Design Life:

A standard shaft is taken to be $8,160 \mathrm{~kg}$.Supported by shaft load studies antecedently undertaken in Bangladesh

Table 3.2: Vehicle Equivalence Factors

| Vehicle Type | Equivalence Factor |
| :--- | :--- |
| Large truck (dual axle) | 4.8 |
| Medium truck(single axle) | 4.62 |
| Small truck | 1.0 |
| Large Bus | 1.0 |
| Mini Bus | 0.5 |

To get the additive ESA loading over the planning lifetime of the road the present annual ESA loading ought to be increased by one of the subsequent factors.

Table 3.3: Cumulative Growth Factors

| Road Type | Factor |
| :---: | :---: |
| National Road | 57.3 |
| Regional Road | 41.0 |

Cumulative ESA $=\frac{(1+r)^{n}-1}{r}$
Where $r=$ annual traffic growth rate
$\mathrm{n}=$ design life in years
Note: for national roads $r=10 \%$ and foe regional roads $r=7 \%$

Table 3.4: Calculating Total ESA

| Vehicle Tpye | Existing <br> Flow/day | ESA Factors | ESA/day | Annual ESAs |
| :---: | :---: | :---: | :---: | :---: |
| Large truck | 606 | 4.8 | 2909 | 1061785 |
| Medium truck | 4258 | 4.62 | 19672 | 7180280 |
| Small truck | 2204 | 1.0 | 2204 | 804460 |
| Large bus | 85 | 1.0 | 85 | 31025 |
| Mini bus | 1199 | 0.5 | 600 | 219000 |
| Car | 2916 | 0.5 | 1458 | 532170 |
| Motor cycle | 1912 | 0.5 | 956 | 348940 |


| CNG | 276 | 0.5 | 138 | 50370 |
| :---: | :---: | :---: | :---: | :---: |
| Micro | 1764 | 0.5 | 882 | 321930 |
|  |  |  | Total | 10549960 |

$$
\begin{aligned}
\text { Cumulative ESAs } & =10549960 * 41 \\
& =432548360 \\
& =432.54 \text { million ESAs }
\end{aligned}
$$

The estimated cumulative ESAs are then used to determine the various pavement layers from the following design chart:


Table 3.1: Thickness Design Table for Flexible Pavements
From the above table we can see that the highest value of ESA is $60-80$ million ESAs but we got the higher than this for that we cannot use this method for high traffic volume because this method is applicable for low traffic volume.

### 3.1.2 AASHTHO method for flexible pavement

Figure below is a pavement system with the resilient module, layer co efficient and drainage coefficient as shown. If predicted ESAL $=18.6 x \mid 0^{6}, \mathrm{R}=95 \%$, $\mathrm{s} .=0.35$ and $\Delta$ PSI $=2.1$, select thickness D1, D2, D3

\[

\]

Sol: calculation of D 1 , here $\mathrm{Mr}=250000 \mathrm{psi}$
We have equation: $\log (\mathrm{W} 18)=\mathrm{Zr}^{*} \mathrm{~S} .+9.36 \log (\mathrm{SN}+1)-0.20+\frac{\log \left(\frac{\Delta P S I}{4.2-1.5}\right)}{0.40+\frac{1094}{(S N+1)^{5.19}}}+2.32 \log \left(\left(M_{R}\right)-\right.$ 8.07
here, $w_{18}=18.6 \quad{ }^{x} 10^{6}$ and for $\mathrm{R}=95 \%, \mathrm{ZR}=-1.645$, $\mathrm{So}=0.35$ and $\mathrm{APSI}=2.1$ then putting these values,
we get,
$\log \left(18.6 \quad{ }^{x} 10^{6}\right)$
$=-1.645 \times 0.35+9.36 \log \left(\mathrm{SN}_{1}+1\right)-0.20++\frac{\log \left(\frac{2.1}{4.2-1.5}\right)}{0.40+\frac{109}{(S N+1)^{5.19}}}+2.32 \log ((250000)-8.07$

So, SN1 $=1.420$
$\mathrm{D} 1=\frac{S N_{1}}{a_{1}}=\frac{1.420^{-}}{0.36}=3.944$ inches
calculating D2: here $M_{R}=100000 \mathrm{psi}$

We have equation: $\log (\mathrm{W} 18)=\mathrm{Zr}^{*} \mathrm{~S} .+9.36 \log (\mathrm{SN}+1)-0.20+\frac{\log \left(\frac{\Delta P S I}{4.2-1.5}\right)}{0.40+\frac{1044}{(S N+1)^{5.19}}}+2.32 \log \left(\left(M_{R}\right)-\right.$ 8.07
here, $w_{18}=18.6{ }^{x} 10^{6}$ and for $\mathrm{R}=95 \%, \mathrm{ZR}=-1.645$, $\mathrm{So}=0.35$ and $\mathrm{APSI}=2.1$ then putting these values, we get,
$\log \left(18.6 \quad{ }^{x} 10^{6}\right)$
$=-1.645 \times 0.35+9.36 \log \left(\mathrm{SN}_{1}+1\right)-0.20++\frac{\log \left(\frac{2.1}{4.2-1.5}\right)}{0.40+\frac{109}{(S N+1)^{5.19}}}+2.32 \log ((100000)-8.07$

So, SN2 $=2.0359$
$\mathrm{D} 2=\frac{S N_{2}-\mathrm{a} 1 * \mathrm{D} 1}{\mathrm{a} 2 * \mathrm{~m} 2}=\frac{2.0359-0.36 * 3.944}{0.12 * 0.12}=4.27$ inches
calculating D3: here $M_{R}=5000 \mathrm{psi}$
We have equation: $\log (\mathrm{W} 18)=\mathrm{Zr}^{*} \mathrm{~S} .+9.36 \log (\mathrm{SN}+1)-0.20+\frac{\log \left(\frac{\Delta P S I}{4.2-1.5}\right)}{0.40+\frac{1094}{(S N+1)^{5.19}}}+2.32 \log \left(\left(M_{R}\right)-\right.$
8.07
here, $w_{18}=18.6 \quad{ }^{x} 10^{6}$ and for $\mathrm{R}=95 \%, \mathrm{ZR}=-1.645$, $\mathrm{So}=0.35$ and $\mathrm{APSI}=2.1$ then putting these values,
we get,
$\log \left(18.6 \quad{ }^{x} 10^{6}\right)$
$=-1.645 \times 0.35+9.36 \log \left(\mathrm{SN}_{1}+1\right)-0.20++\frac{\log \left(\frac{2.1}{4.2-1.5}\right)}{0.40+\frac{1094}{(S N+1)^{5.19}}}+2.32 \log ((5000)-8.07$

So, SN3 $=5.377$
$\mathrm{D} 3=\frac{S \mathrm{~N} 3-\mathrm{a} 1 * \mathrm{D} 1-\mathrm{a} 2 * \mathrm{D} 2 * \mathrm{M} 2}{\mathrm{a} 3 * \mathrm{~m} 3}=\frac{5.377-0.36 * 3.944-0.12 * 4.278 * 1.2}{0.08 * 1.2}=34.80$ inches

### 3.1.3 Flexible pavement design:

Design flexible pavement for an undivided rural highway by using Catalogue of Pavement Structures

Method for the following data.
Table 3.2:

| VEHICLE type | AADT |
| :--- | :--- |
| Large truck | 606 |
| Small truck | 2204 |
| Large bus | 85 |
| Small bus | 1764 |
| car | 2916 |
| Auto rickshaw | 1767 |
| Motor cycle | 1912 |
| Bi cycle | 17 |

Solution:

Table 1: PCU Factors for Rural Road

| Vehicle Types | PCU Factors |  |  |
| :---: | :---: | :---: | :---: |
| Large Truck | 3.0 |  |  |
| Small Truck | 2.0 |  |  |
| Large Bus | 2.5 |  |  |
| Small Bus | 1.5 |  |  |
| Car/Tempo | 1.0 |  |  |
| Autorickshaw | 0.5 |  |  |
| Motor Cycle | 0.3 |  |  |
| Bicycle | 0.3 |  |  |
| Rickshaw | 2.0 |  |  |
| Cart | 4.0 |  |  |
|  |  |  |  |

Table 3.3:

| Vehicle type | AADT | PCU factors | Traffic volume * <br> PCU factors |
| :--- | :--- | :--- | :--- |
| Large truck | 606 | 3.0 | 1818 |
| Small truck | 2204 | 2.0 | 4408 |
| Large bus | 85 | 2.5 | 212.5 |
| Small bus | 1764 | 1.5 | 2650.5 |
| car | 2916 | 1.0 | 2916 |
| Auto rickshaw | 1767 | 0.5 | 883.5 |
| Motor cycle | 1912 | 0.3 | 573.6 |
| Bi cycle | 12 | 0.3 | 5.1 |
|  |  |  | Total= |

Forecasted design flow $=13467.2 *(1+r)^{n}$
$13467.2 *(1+0.08)^{20}=62770.04 \mathrm{pcu} /$ day


So we can see our design forecast flow is not matching with any optimum design capacity so that it is impossible to choose a cross section.

So this method is impossible.

## Usefulness of flexible pavement:

Flexible usually applied in thick layer which gives it the ability to withstand heavy load and more traffic flows. So for major roadway engineer chose this pavement system. Flexible pavement requires regular maintainance but it is fairly easy to do.

Problems of flexible pavement:
As we have mentioned flexible pvament needs regular maintainance. If not than there are few problems can be seen. Like-

- Bleeding in Flexible Pavements.
- Block Cracking in Flexible Pavements. This is also called as thermal cracking.
- Bumps and Sags.
- Edge Cracking in Flexible Pavements.
- Joint Reflection Cracking.
- Raveling.
- Cold Joints in Flexible Pavements.
( source : google)


### 3.1.4 Pavement design for rigid pavement:

Rigid pavements are constructed of portland cement concrete( PCA) slabs resting on a prepared subbase of granular material or directly on a granular subgrade. Load is transmitted through the slabs to the underlying subgrade by flexure of the slabs.
(source: google)


Subgrade: subgrade can be earth or soil. It is the base layer the pavement.
Subbase: it can be hard earth or stone. This part is just over part of subbase layer. This part is not mandatory to give.

Base course: this part consist of granular crushed stone or chip stone.
Concrete slab: this part is RCC structure. This is the top of all the layers.

## PCA Design method:

Two types of failure mode considered
1.Fatigue failure
2. Erosion failure

## Design parameters:

1. Concrete modulus of rupture (MR)
2. Modulus of subgrade reaction (k)
3. Design traffic volume
4. Axle load spectrum

## Design procedure:

- Choose a trial slab thickness
- Calculate the fatigue and erosion failure
- Sum of fatigue and erosion failure of the axle load classes


## Data Analysis:

Annual Average Daily Traffic :17074 from which we can assume the data was collected at the month of August for that we can now calculate ADT which is
$\frac{A A D T}{M E F}=\frac{17074}{0.521}=32772$
Percentage of truck determination:

| Vehicle type | Number <br> ofvehicle | Percentage |
| :--- | :--- | :--- |
| Large bus | 85 | 0.55 |
| Mini bus | 1199 | $7 . .87$ |
| Private car | 2919 | 19.17 |
| Motor cycle | 1912 | 12.56 |
| CNG | 276 | 1.81 |
| Micro | 1764 | 46 |
| Truck | 7068 |  |
| Total | 15223 |  |

Growth Rate : 7\%

Design Year : 20 years
Direction Distribution factor : 0.5
Clay sub-grade, $\mathbf{k}=100 \mathrm{psi} /$ in (assume)
Concrete MR $=650 \mathrm{psi}$ (assume)
Use subbase $=4$ " untreated (assume)
Use Doweled JPCP and Asphalt shoulders
Traffic Growth Multiplier:

$$
\mathbf{G}=(1+r)^{Y / 2}=1.97
$$

Lane Distribution Factor: $(\mathrm{ADT})^{*}(\mathrm{D}) *(\mathrm{G})=32772 * 0.5^{*} 1.97=32280$


Figure: Lane Distribution Factor

From the above figure we can say the of $L=0.73$

## Design traffic Volume:

$$
\begin{aligned}
\mathbf{V} & =365 *(\mathrm{ADT}) *(\mathrm{~T}) *(\mathrm{D})^{*}(\mathrm{~L}) *(\mathrm{G}) *(\mathrm{Y}) \\
& =78046308 \text { truck }
\end{aligned}
$$

| Subgrade | Subbase k value,pci |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| k value, <br> pci | 4 in | 6 in | 9 in | 12 in |
| 50 | 65 | 75 | 85 | 110 |
| 100 | 130 | 140 | 160 | 190 |
| 200 | 220 | 230 | 270 | 320 |
| 300 | 320 | 330 | 370 | 430 |

Table: Design K value for untreated subbase

When

Subgrade K = 100 psi
Untreatedsubbase : 4 in

So the subgrade k value from table is : 130 psi

| Traffic volume | LSF |
| :---: | :---: |
| High |  |
| (interstates, multilane highways) | 1.2 |
| Moderate |  |
| (highways and arterials) | 1.1 |
| Low |  |
| (collectors, residential streets) | 1.0 |

Table : Load safety Factor

## For Both Axle :

Subbase subgrade $\mathbf{k}=130 \mathrm{psi}$
Slab thickness $=9.5$ in

| Equivalent Stress - No Concrete Shoulder (Single Axle / Tandem Axle) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Slab thickness, in. | $k$ of subģrade-subsase, pci |  |  |  |  |  |  |
|  | 50 | 100 | 150 | 200 | 300 | 500 | 700 |
| 4 | 825/679 | 726/585 | 671/542 | 634/516 | 584/486 | 523/457 | 484/443 |
| 4.5 | 699/586 | 616/500 | 571/460 | 540/435 | 498/406 | 448/378 | 417/363 |
| 5 | 602/516 | 531/435 | 493/399 | 467/376 | 432/349 | 390/321 | 363/307 |
| 5.5 | 526/461 | 464/387 | 431/353 | 409/331 | 379/305 | 343/278 | 320/264 |
| 6 | 465/416 | 411/348 | 382/316 | 362/296 | 336/271 | 304/246 | 285/232 |
| 6.5 | 417/380 | 367/317 | 341/286 | 324/267 | 300/244 | 273/220 | 256/207 |
| 7 | 375/349 | 331/290 | 307/262 | 292/244 | 271/222 | 246/199 | 231/186 |
| 7.5 | 340/323 | 300/268 | 279/241 | 265/224 | 246/2C3 | 224/181 | 210/169 |
| ¢ | 311/300 | 274/249 | 255/223 | 242/208 | 225/188 | 205/167 | 152:155 |
| H. 5 | 235/261 | 252/232 | 234/208 | 222/193 | 206/174 | 188/154 | 177/143 |
| 9 | 254/264 | 232/218 | 216/195 | 205/181 | 190/163 | 174/144 | $163!133$ |
| $9.5$ | 245/248 | 215/205 | 200/183 | 190/170 | 176/153 | 161/134 | 151/124 |
| $10$ |  | 203/193 | $186 / 173$ | 177/160 | 164/144 | 153/126 | 141/117 |
| $10.5$ | $213 / 222$ | 187/183 | 174/164 | 165/151 | 153/136 | 140/119 | 132/110 |
| 11 | 200/211 | 175/174 | 163/155 | 156/143 | 144/129 | 131/113 | 123/104 |
| 11.5 | i88/20i | 1651165 | 153/1:8 | 145/136 | 135/122 | 123/137 | 116/®0 |
|  |  | 155/158 | 164/141 | 137/130 | 127/116 | $116 / 102$ | 109/93 |
| $12.5$ | $158 / 183$ | $147 / 151$ | 136/135 | 129/124 | 120/111 | 109/97 | 103/29 |
| 13 |  |  |  |  |  | $103 / 93$ | $97 / 05$ |
| 13 13.5 | $\begin{aligned} & 159 / 176 \\ & 152 / 168 \end{aligned}$ | $132 / 138$ | $122 / 123$ | $116 / 114$ | $107 / 1 \mathrm{C} 2$ | $98 / 89$ | $02 / 81$ |
| 13.5 |  |  | i15/118 | 110;109 | 102/98 | $93 / 85$ | ¢8/78 |
| 14 | 144/162 | 125:133 | 115/118 | $110 / 109$ | 102.9 |  |  |

Erosion Factor－Doweled Joints，No Concrete Shoulder （Single Axle／Tandem Axle）

| Stab thickness． ＇n． | k ol subcrade－subbase，del |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 100 | 200 | 300 | 500 | 700 |
| 4 | 3．74／3 83 | 3．73．3．79 | 3．72／3．75 | 3．71／373 | 37013.70 | 2．68／367 |
| 4.5 | 3．59／3．70 | 3．57／3．65 | 3．56／3．61 | $3.55 / 358$ | $354 / 3.55$ | 3．52／3．53 |
| 5 | $345 / 3.58$ | 3．43．3 52 | $3.42 / 3.48$ | 3．41／3．45 | $3.40 / 3.42$ | 3．38／3．40 |
| 55 | $3.33 / 3.47$ | $3.31: 3.41$ | 3．29／3 35 | 3．28／3 33 | 3．27，3．30 | 3． $26 / 328$ |
| 5 | $3.22 / 3.38$ | $3.19 / 3.31$ | 3．18：3．26 | 3．17／323 | $315 / 3.20$ | 3．4／3．17 |
| 65 | 311.3 .29 | $309 / 3.22$ | $307 / 316$ | 3．06／3 13 | 305：3．10 | 3 03／307 |
| 7 | $3.02 / 3.21$ | $299 / 3.14$ | $297 / 308$ | $2.95 / 305$ | 29513.01 | 2．94，298 |
| 7.5 | $293 / 314$ | 2．91．306 | 2．88．3．03 | 2．87／2．97 | 286.2 .93 | 2．34／290 |
| $8$ | $2.85 / 3.67$ | $2.82: 2.99$ | $280 / 293$ | $279: 249$ | $277 / 2.85$ | ？76：2．82 |
| $\text { B } 5$ | $277 / 3.01$ | $2.14: 2.93$ | $272: 2.86$ | $2.71 / 262$ | 269.278 | 2．08．2．75 |
| 9 | $2.70 / 296$ | $267 / 287$ | $265^{\prime} 2.80$ | 2．63275 | $25227$ | $\text { 2. } 61 / 2.68$ |
| $95$ | 2．93／290 | $2601281$ | $258 \cdot 2.75$ | 256／270 | $255^{\prime 2} .65$ | $\text { 2. } 54 / 2.62$ |
| 10 | $256 / 285$ | 254：276 | 2こ1：266 | $2.50 / 264$ | $248: 2.59$ | 2．67i256 |
| 105 | 250／2．81 | 2．471271 | 245／263 | $244 / 259$ | 242.2 .54 | 2．41／251 |
| 11 | 24.42 .76 | 2.421297 | $239 / 259$ | $2.38 \cdot 2.54$ | $236 / 249$ | 235.2 .45 |
| 115 | $238 / 272$ | ？36．2．5．？ | 2 3iv： 54 | $232: 249$ | $230 \cdot 246$ | ？29：2 40 |
| 12 | 233／26E | 2．30：2．58 | 2．25．2．49 | $226 / 244$ | $225 \% 39$ | 2．23：2．35 |
| 125 | 228.264 | 225：254 | 2 23：2 45 | 221／240 | 2．19：2 35 | 218123 |
| 13 | $223 / 26:$ | 2．20：250 | $218^{\prime 2} 4.47$ | 2．16．236 | $2 \cdot 4.2 .30$ | 213.227 |
| 13.5 | $218 / 2.57$ | $2 \cdot 51247$ | 213\％37 | 2．11／2 32 | $709 / 226$ | 2 （18：2 23 |
| 14 | $213{ }^{\prime} 254$ | $2: 1: 243$ | 358.234 | 23フ／229 | こ05 27 | 235219 |

## Single Axle ：

＊Equivalent Stress ： 206 （using interpolation）
＊Stress Ration factor ：$\frac{206}{M r}=\frac{206}{650}=0.317$

## Tandem Axle ：

＊Equivalent Stress ： 192 （using interpolation）
＊Stress Ration factor ：$\frac{190}{M r}=\frac{190}{650}=0.295$


Figure : Fatigue Analysis Based on Stress ratio factor


Table :Damage analysis Based on Erosion Factor

Table : Single Axle load

| Axle load <br> kips | LSF | Multiplied <br> By LSF | Expected <br> repetition | Fatigue Analysis <br>  |  | Allowable <br> repetition | Fatigue <br> percent |
| :---: | :---: | :---: | :--- | :--- | :--- | :--- | :--- |
| 30 | 1.2 | 36 | 6310 | 27000 | 23.34 | Allowable <br> repetitions | Demage <br> percent |
| 28 | 1.2 | 33.6 | 14690 | 79000 | 18.60 | 2500000 | 0.59 |
| 26 | 1.2 | 31.2 | 30140 | 220000 | 13.7 | 7000000 | 0.75 |
| 24 | 1.2 | 28.8 | 64410 | 1800000 | 3.58 | 15000000 | 0.92 |
| 22 | 1.2 | 26.4 | 106900 | unlimited | 0.00 | 25000000 | 0.71 |
|  |  |  |  | total | 59.28 | 80000000 | 0.94 |
|  |  |  |  |  |  | Unlimited |  |
|  |  |  |  |  |  | total | 4.62 |

Table : Tandem Axle load

| Axle <br> load <br> kips | LSF | Multiplied <br> By LSF | Expected repetition | Fatigue Analysis |  | Erosion Analysis |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Allowable repetition | Fatigue percent | 970000 | 2.19 |
| 52 | 1.2 | 62.4 | 21320 | 1100000 | 1.9 | 1900000 | 2.25 |
|  |  |  |  | unlimited |  | 2500000 | 5 |
|  |  |  |  | total | 61.18 | 4600000 | 8.1 |
|  |  |  |  |  |  | 9500000 | 9.3 |
|  |  |  |  |  |  | 24000000 | 3.9 |
|  |  |  |  |  |  | 92000000 | 1.8 |
|  |  |  |  |  |  | Unlimited | 0.0 |
|  |  |  |  |  |  | total | 32.57 |
|  |  |  |  | $\begin{aligned} & \text { Total } \\ & 61.18 \end{aligned}$ |  | $37.19$ |  |

## Comments :

Total Fatigue and Damage $=$ Fatigue $\%+$ Damage $\%$

$$
\begin{aligned}
& =61.18+37.19 \\
& =98.37 \%
\end{aligned}
$$

Which is acceptable
Therefore Design thickness, $\mathrm{t}=9.5$ in

## Notes :

* If total fatigue and damage was $\ll 100 \%$;
which would have implied that the assumed thickness was overestimated. As such, 2nd trial would have been needed with reduced thickness.

If total fatigue and damage was $\gg 100 \%$; which would have implied that the assumed thickness was under-estimated. As such, 2nd trial would have been needed with increased thickness.

### 3.1.5 AASHTO Rigid Pavement Design

Analysis: A rigid pavement is to be designed to provide a service life of 20 years and has an initial

PSI of 4.4 and a TSI of 2.5. The modulus of subgrade reaction is determined to be 300 $\mathrm{lb} / \mathrm{in}^{3}$. For design, the daily car, pickup truck, and light van traffic is 5120 ; and the daily truck traffic consists of 4864 passes of single-unit trucks with single and tandem axles, and . The axle
weights are
cars, pickups, light vans $=$ two $2000-\mathrm{lb}$ single axles
single-unit trucks $=10,000-\mathrm{lb}$ steering, single axle
$22,000-\mathrm{lb}$ drive, tandem axle

Reliability is $95 \%$, the overall standard deviation is 0.45 , the concrete's modulus of elasticity is 4.5 million $\mathrm{lb} / \mathrm{in}^{2}$, the concrete's modulus of rupture is $900 \mathrm{lb} / \mathrm{in}^{2}$, the load
transfer coefficient is 3.2 , and the drainage coefficient is 1.0. Determine the required slab thickness.

## Solution:

Because the axle-load equivalency factors presented in Tables are function of the slab thickness (D), we have to assume a D value to start the problem (later we will arrive at a slab thickness and check to make sure that it is consistent with our assumed value). A typical assumption is to let $\mathrm{D}=10$ inches. Given this, the 18-kipequivalent single-axle load (18-kip ESAL) for cars, pickups, and light vans is 2-kip single-axle equivalent $=0.0002$ (from the table)

Table 4.6 Axle-Load Equivalency Factors for Rigid Pavements, Single Axles, and TSI = 2.5

| Axle load (kins) | Slab thickness, $D$ (inches) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 2 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 | 0.0002 |
| 4 | $0.003$ | 0.002 | 0.002 | 0.002 | -0.00 | 0.002 | $0.002$ | $0.002$ | $0.002$ |
| 6 | 0.012 | 0.011 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 | $0.010$ |
|  | 0.039 | 0.035 | 0.033 | 0.032 |  | 0.032 | 0.032 | 0.032 | 0.032 |
| 10 | $0.097$ | $0.089$ | $0.084$ | 0.082 | 0.081 | $0.080$ | 0.080 | 0.080 | $0.080$ |
| $\cdots$ | $0.203$ | 0.189 | 0.181 | 0.176 |  | 0.174 | 0.174 | 0.174 | $0.173$ |
| 14 | $0.376$ | 0.360 | $0.347$ | $0.341$ | 0.338 | $0.337$ | $0.336$ | $0.336$ | $0.336$ |
| 16 | 0.634 | 0.623 | 0.610 | 0.604 | 0.601 | 0.599 | 0.599 | 0.599 | $0.598$ |
| 18 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 20 | 1.51 | 1.52 | 1.55 | 1.57 | 1.58 | 1.58 | 1.59 | 1.59 | 1.59 |
| 22 | 2.21 | 2.20 | 2.28 | 2.34 | 2.38 | 2.40 | 2.41 | 2.41 | 2.41 |
| 24 | $3.16$ | 3.10 | 3.22 | $3.36$ | $3.45$ | 3.50 | 3.53 | 3.54 | $355$ |
| $26$ | 4.41 | 4.26 | 4.42 | 4.67 | 4.85 | 4.95 | 5.01 | 5.04 | $5.05$ |
| 28 | $6.05$ | 5.76 | 5.92 | $6.29$ | 6.61 | 6.81 | 6.92 | 6.98 | 7.01 |
| 30 | 8.16 | 7.67 | 7.79 | 8.28 | 8.79 | 9.14 | 9.35 | $9.46$ | $9.52$ |
| 32 | 10.8 | 10.1 | 10.1 | 10.7 | 11.4 | 12.0 | 12.3 | 12.6 | $12.7$ |
| 34 | 14.1 | 13.0 | 12.9 | 13.6 | $14.6$ | 15.4 | 16.0 | 16.4 | $16.5$ |
| 36 | 18.2 | 16.7 | 16.4 | 17.1 | 18.3 | 19.5 | 20.4 | 21.0 | 21.3 |
| 38 | 23.1 | 21.1 | 20.6 | 21.3 | $22.7$ | 24.3 | 25.6 | 26.4 | $27.0$ |
| 40 | 29.1 | 26.5 | 25.7 | 26.3 | 27.9 | 29.9 | 31.6 | 32.9 | 33.7 |
| 42 | 36.2 | 32.9 | 31.7 | $32.2$ | $34.0$ | 36.3 | $38.7$ | 40.4 | $41.6$ |
| 44 | 44.6 | 40.4 | 38.8 | 39.2 | 41.0 | 43.8 | 46.7 | 49.1 | 50.8 |
| 46 | 54.5 | 49.3 | 47.1 | 47.3 | 49.2 | 52.3 | 55.9 | $59.0$ | 61.4 |
| 48 | 66.1 | 59.7 | 56.9 | 56.8 | $58.7$ | 62.1 | 66.3 | 70.3 | $73.4$ |
| 50 | 79.4 | 71.7 | 68.2 | 67.8 | 69.6 | 73.3 | 78.1 | 83.0 | 87.1 |

Source: AASHTO Guide for Design of Pavement Structures, The American Association of State Highway and Transportation Officials, Washington, DC, 1993. Used by permission.

Table 4.7 Axle-Load Equivalency Factors for Rigid Pavements, Tandem Axles, and TSI = 2.5

| Axle load (kips) | Slab thickness, $D$ (inches) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | $7$ | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 2 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 | 0.0001 |
| 4 | 0.0006 | 0.0006 | 0.0005 | 0.0005 | 0.0005 | 0.0005 | 0.0005 | 0.0005 | 0.0005 |
| 6 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8 | 0.007 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 10 | 0.015 | 0.014 | 0.013 | 0.013 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 12 | 0.031 | 0.028 | 0.026 | 0.006 | 0.025 | 0.005 | 0.005 | 0.025 | 0.025 |
| 14 | 0.057 | 0.052 | 0.069 | 0.048 | 0.047 | 0.047 | 0.047 | 0.047 | 0.047 |
| 16 | 0.097 | 0.089 | 0.084 | 0.082 | 0.081 | 0.081 | 0.080 | 0.080 | 0.080 |
| 18 | 0.155 | 0.143 | 0.136 | 0.133 | 0.132 | 0.131 | 0.131 | 0.131 | 0.131 |
|  | 0.234 | 0.220 | 0.211 | 0.206 |  | 0.203 | 0.203 | 0.203 | 0.203 |
| 22 | 0.340 | 0.325 | 0.313 | 0.308 | 0.305 | 0.304 | 0.303 | 0.303 | 0.303 |
|  | 0.475 | 0.462 | 0.450 | 0.444 | +1 | 0.440 | 0.439 | 0.439 | 0.439 |
| 26 | 0.644 | 0.637 | 0.627 | 0.622 | 0.629 | 0.619 | 0.618 | 0.618 | 0.618 |
| 28 | 0.855 | 0.854 | 0.852 | asso | 0.850 | 0.850 | 0.869 | 0.849 | 0.849 |
| 30 | 1.11 | 1.12 | 1.13 | 1.14 | 1.14 | 1.14 | 1.14 | 1.14 | 1.14 |
| 32 | 1.43 | 1.44 | 1.47 | 1.49 | 1.50 | 1.51 | 1.51 | 1.51 | 1.51 |
| 34 | 1.82 | 1.82 | 1.87 | 1.92 | 1.95 | 1.96 | 1.97 | 1.97 | 1.97 |
| 36 | 2.29 | 227 | 235 | 2.43 | 2.48 | 2.51 | 2.52 | 2.52 | 2.53 |
| 38 | 2.85 | 2.80 | 291 | 3.03 | 3.12 | 3.16 | 3.18 | 3.20 | 3.20 |
| 40 | 3.52 | 3.42 | 3.55 | 3.74 | 3.87 | 3.94 | 3.98 | 4.00 | 4.01 |
| 42 | 4.32 | 4.16 | 4.30 | 4.55 | 4.74 | 4.86 | 4.91 | 4.95 | 4.96 |
| 44 | 5.26 | 5.01 | 5.16 | 5.48 | 5.75 | 5.92 | 6.01 | 6.06 | 6.09 |
| 46 | 6.36 | 6.01 | 6.14 | 6.53 | 6.90 | 7.14 | 7.28 | 736 | 7.40 |
| 48 | 7.64 | 7.16 | 727 | 7.73 | 8.21 | 8.55 | 8.75 | 8.86 | 8.92 |
| 50 | 9.11 | 8.50 | 8.55 | 9.97 | 968 | 10.14 | 10.42 | 10.58 | 10.66 |
| 52 | 10.8 | 10.0 | 10.0 | 10.6 | 113 | 11.9 | 12.3 | 125 | 127 |
| 54 | 12.8 | 11.8 | 11.7 | 123 | 13.2 | 13.9 | 14.5 | 14.8 | 14.9 |
| 56 | 15.0 | 13.8 | 13.6 | 14.2 | 15.2 | 16.2 | 16.8 | 17.3 | 17.5 |
| 58 | 17.5 | 16.0 | 15.7 | 16.3 | 175 | 18.6 | 19.5 | 20.1 | 20.4 |
| 60 | 20.3 | 18.5 | 18.1 | 18.7 | 20.0 | 21.4 | 22.5 | 23.2 | 23.6 |
| 63 | 23.5 | 21.4 | 20.8 | 21.4 | 228 | 24.4 | 25.7 | 26.7 | 27.3 |
| 64 | 27.0 | 24.6 | 23.8 | 24.4 | 25.8 | 27.7 | 29.3 | 30.5 | 31.3 |
| 66 | 31.0 | 28.1 | 27.1 | 27.6 | 29.2 | 31.3 | 33.2 | 34.7 | 35.7 |
| 68 | 35.4 | 32.1 | 309 | 31.3 | 32.9 | 35.2 | 37.5 | 39.3 | 40.5 |
| 70 | 40.3 | 36.5 | 35.0 | 35.3 | 37.0 | 39.5 | 42.1 | 44.3 | 45.9 |
| 72 | 45.7 | 41.4 | 39.6 | 39.8 | 41.5 | 44.2 | 47.2 | 49.8 | 51.7 |
| 74 | 51.7 | 46.7 | 44.6 | 44.7 | 46.4 | 49.3 | 52.7 | 55.7 | 58.0 |
| 76 | 58.3 | 52.6 | 50.2 | 50.1 | 51.8 | 54.9 | 58.6 | 62.1 | 64.8 |
| 78 | 65.5 | 59.1 | 563 | 56.1 | 57.7 | 60.9 | 65.0 | 69.0 | 723 |
| 80 | 73.4 | 66.2 | 629 | 62.5 | 64.2 | 675 | 71.9 | 76.4 | 30.2 |
| 82 | 82.0 | 73.9 | 70.2 | 69.6 | 71.2 | 74.7 | 79.4 | 84.4 | 88.8 |
| 84 | 91.4 | 82.4 | 7 T .1 | 77.3 | 78.9 | 82.4 | 87.4 | 93.0 | 98.1 |
| 86 | 102.0 | 920 | 87.0 | 86.0 | 87.0 | 91.0 | 96.0 | 102.0 | 1080 |
| 88 | 113.0 | 1020 | 960 | 95.0 | 960 | 1000 | 105.0 | 1120 | 119.0 |
| 90 | 125.0 | 112.0 | 106.0 | 105.0 | 106.0 | 110.0 | 115.0 | 123.0 | 130.0 |

Source: AASHTO Guide for Design of Pavement Sinuctures, The American Association of Stale Mighway and Tramportation Officials, Washington, DC, 1993. Used by permission.

This gives an 18-kip ESAL total of 0.0004 for each vehicle. For single-unit trucks, 10-kip single-axle equivalent $=0.081$ (from the table)

22 -kip tandem-axle equivalent=0.305 (from the table)

This gives an 18-kip ESAL total of 0.386 for single-unit trucks.

Given the computed 18-kip ESAL, the daily traffic on this highway produces an 18-kip ESAL total of 1879.552 ( $0.0004 \times 5120+0.386 \times 4864$ ). Traffic (total axl accumulations) over the 20-year design period will be $1879.552 \times 365 \times 20=13720729.6$ 18-kip ESAL

Here $w_{18}=13720729.6$
$\mathrm{Z}=0.95$
$s_{0}=0.45$
TSI $=2.5$
$\Delta \mathrm{PSI}=1.9$
$s_{c}^{\prime}=900$
$C_{d}=1$
$\mathrm{J}=3.2$
$E_{C_{-}}=4.5$ million
$\mathrm{K}=300$



So from the nomograph we can get $\mathrm{D}=8.5$ inches

## Usefulness of rigid pavement:

Since rigid pavement consist of RCC work, it remains more durable over the time. It does not bend for heavy load and regular maintenance is not necessary and it is less expensive.

## Disadvantages of rigid pavement:

Since it is RCC work, curing time is 28 days so that road remains off for a long time.

## Chapter 4

## Transportation Road Safety

## Introduction

For predominantly humanitarian, health, and financial reasons, nations place a high focus on the case of road safety. As stated by the 'World Health Organization(WHO)',Around 1.3 million individuals per year perish due to road accidents., just around 3400 deadly accidents everyday, and, in addition, around 30 and 50 million people face non destructive injuries annually . It is possible to pinpoint,and survey the damaging points of accidents ,utilizing resources like the Institution of Highways Transportation's Highway safety protocols: Accident prevention and elimination. This is one of the most effective approaches to the prevention of traffic accidents.

## Why is road safety important

Road safety is using all available road safety measures to avoid and protect against traffic accidents. Road safety is ensured when someone is driving on a roadway. All users of the road, including pedestrians and users of two-, four-, multi-, and other transport vehicles, must be protected.It is beneficial and safe for everyone to practice road safety precautions throughout their lives. While driving or walking on the road, everyone should show consideration for others and guarantee their safety. One of the most critical factors in stemming roadside accidents, harm, and fatalities is ensuring that people are safe while driving. Based on national statistical data regarding the total number of reported casualties and fatalities, we may assess the significance of road safety. Road accidents can be significantly reduced by following all traffic safety precautions. Basic vehicle knowledge, defensive driving by weather and roadway conditions, the usage of automotive body lights and horns, using a seat-belt, making good usage of automotive looking glasses, avoiding excessive acceleration, comprehension of road lights, maintaining a safe following distance, knowing how to handle emergencies, broadcasting awareness tv
programs on Broadcast, and so on. seem to be some effective methods of road safety. Road Safety regulations are designed to reduce the likelihood of accidents. Every day, millions of automobiles travel the world's roads. Because of this, there ought to rule that must be adhered to when using the roadways.

Humans and automobiles can both benefit from these guidelines. Following all road safety measures will go a long way in preventing all road problems. Some effective road safety measures are basic vehicle recognition, protection, etc. Driving in climatic and street condition, using car light and horns, using Proper seat belts, and vehicle mirrors, avoiding excessive speed, understanding street lights, maintaining vehicle distance on the road, and correct understanding of how to deal with crises, television broadcastingAwareness-raising documentaries on TV, etc. Traffic safety rules are in place to contain opportunities for the traffic accident. Millions of vehicles regularly move on our roads. that's why they're a set of rules that must be observed when using the road. These rules not only applies not only to cars but also to people walking or biking on the street results. Road safety rules are important for many reasons. There are various traffic safety rules for motorcycles, passenger cars, trucks, tractors, etc. Driver's license and car license plate is valid evidence. Properly identified vehicles serve as protection for road transport. Most accidents are caused by the high speed of the vehicle. to reduce irresponsible behavior of driving where traffic safety rules are in place. implemented by the government Various strict rules for vehicles. Drivers must obey traffic lights and signs near schools. hospitals and other public places.

## Road safety rules

Vehicle traffic safety regulations state:

- Always stop your vehicle at red lights.
- Avoid using your mobile phone while driving.
- Do not cross before the light turns green.
- Always leave space for unauthorized persons.
- Do not ride on footbridges or sidewalks.
- Wear a helmet when riding a motorcycle.
- Wear seat belts when riding in a four-wheeled vehicle.
- Always carry your driver's license and important vehicle documents with you while driving.
- Do not drive under the influence of alcohol or drugs. $\cdot$ Slow down when crossing pedestrian crossings.
- Obey signs and instructions near hospitals and schools.
- Do not attempt to pass ambulances or other emergency vehicles.

Awareness and traffic safety rules are linked. When people realize the importance of life, The probability of traffic accidents is automatically reduced. Observance of traffic safety rules being a citizen of a particular country also helps reduce the chances of road traffic accidents. Traffic safety rules are also one of the manners that can be incorporated into daily life. when we are time management helps when you run out of time. Need traffic safety rules for all of us. In short, traffic safety rules are life-saving disciplines that must be strictly adhered to Note.

## ROAD INFRASTRUCTURE AND STREET PROTOCOLS

Road geometry plays an important role in the frequency and rate of traffic accidents. car accident severity. Various fundamentals of street design are important. However, some boundaries are regarded to be more pronounced and are talked about below.

## Road way crosssection

Lane width not only affects driving and maneuvering comfort It is a characteristic of the road surface, but it is also an important parameter that influences the frequency of traffic accidents, and crash seriousness. For each useful classification of road, it may be a trunk road, For each road environment, rural roads, and whether urban or country roads, Lane width narrows, greatly increasing the probability of an accident. for example, A study of safety issues on an undivided two-lane highway found the lanes to be wider and decrease the likelihood of head-on or other related collisions from 2.

75 meters to 3.65 meters $50 \%$ ( $50 \%$ ). 5 Increased traffic and narrower lane widths reduce the probability of accidents. In particular, accidents such as head-on collisions and road deviations are increasing.

The significance of wide hard shoulder is even more precise on two lane roads.A paved shoulder is the best shoulder from a traffic welfare wise and is better than gravel. Gravel shoulders are better than composite shoulders (a combination of different types). However, grass shoulders are considered the worst from a traffic safety viewpoint and can result in a 10 . Percentage ( $10 \%$ ) more crashes.

According to the literature, skidding accidents are a major concern for road safety

## Roadside Conditions

The term "free zone" means the unobstructed passable area that extends beyond the edge of a road. moving vehicle. in some places available right-of-way or width to provide clear space is insufficient or impractical, As expected, we can generally recognize the concept of free zones. Lateral offset is allowed for safety consideration of vertical obstacles (signs, poles, etc.) are required to keep away from collisions. The existence of medians is one of serious factor in accidents, mainly frontal crashes. However, for safety and security reasons, medians are highly desirable on multi-lane highways. operational efficiency.

## Road Curvature

Curve lanes are served with angular features on the curves section of the road known as "Superelevation". i. e. outside the lane Since the curve is higher than the inside, the component of its weight The vehicle prevents the vehicle from moving to the outside.

However, vehicle speed is also an important factor. at a driving speed When the cars crosses the preferred or designated limit of the curve, the car loses control and Serious "runaway" accidents can occur. On the off chance that the progress bend isn't as expected gave, Then a diffusive power is out of nowhere applied to the vehicle, and contingent upon the speed and speedThe weight of your vehicle can make you fail to keep a grip on your vehicle. He could have 15D44 more car crashes on his two-path parkway on steep landscape than on comparable streets on level territory.therefore, Climbing lanes for heavy vehicles (additional lanes) can reduce the chance of an accident on a two-lane section by $25 \%$.

## Sight Distance

Sufficient visibility is required for the driver to control the operation Protect your vehicle from hitting unexpected objects on the road. Passing Visibility should be enabled on two-lane roads Drivers use oncoming traffic to overtake (overtake) other vehicles without hindrance coming cars. The concepts of SSD and PSD are most important from a traffic safety point of view, Decision Sight Distance (DSD) is one more significant issue that should be tended to for individuals' wellbeing. street clients.

Be that as it may, under typical conditions, drivers need longer distances to go with complex choices. DSD is the distance it takes a driver to recognize a startling or difficult to-identify occasion. See sources or conditions in the street climate.

## Road Construction safety Tips

As transportation is very important without them the finencial condition will collapse in a country roads are the main means of transportation. This are the reason why the structure should be taken very seriously. Still every year road workers risk their life in building them. And if not serious and careful we can suffer a serious loss.
some roadworks safety tips for workers:

## A plan

All street development projects require a transportation the executives plan. The arrangement ought to comprise of a brief traffic signal intend to safeguard laborers by securely coordinating traffic around or through the workspace. You likewise need a traffic signal arrangement inside the work zone that controls the progression of weighty gear, development vehicles, and laborers.

## Traffic Control

work area ought to comprise a progressed caution region with caution signs cautioning drivers of up-and-coming changes in driving conditions, a move range utilizing activity control gadgets for path closures and activity design shifts, a buffer region, the working range, and an end region to permit activity to continue to ordinary and a signs showing that the construction area has finished.

## A separate work space

Street development construction areas are active zones as a rule with a few work exercises taking put at the same time. To maintain a strategic distance from mishaps, utilize cones, barrels, and obstructions to depict particular regions of the work area such as fabric capacity, regions where overwhelming hardware is utilized, car stops, and secure ranges for foot specialists to move approximately in.

## Site Safety Program

Every road improvement adventure is different and each work zone has its case of fascinating dangers and difficulties so making a security program prepared especially for the area can go quite far in keeping away from mishaps. The site-explicit security program should consolidate recognizing all dangers and plans to control and direct them, plans to regularly survey all equipment and texture, orchestrate in the first place help and emergency supportive consideration inside the event of a mishap, and security planning plans for all specialists.

## Start workers with safety instructions

As well as guaranteeing that all staff at the Place of work have the legitimate preparation required it is likewise really smart to have a speedy security meeting before work starts. Since conditions can change significantly from one day to another in the work zone, laborers ought to be advised on the work movement booked every day and told of every possible risk. This is likewise a great opportunity to guarantee that all laborers have and are wearing the legitimate PPE expected for the work being done that day.

## Avoid spots that are not visible

Vehicles and weighty gear, for example, dump trucks, compactors, graders, backhoes, pavers, and rollers are continually traveling through the workspace. The administrator should guarantee that all mirrors and visual guides are appropriately situated and working appropriately including reinforcement alerts and lights. Know that the driver's perceivability might be limited while strolling or working close to these machines when they are in activity. Continuously keep visual contact with the driver. As a guideline, on the off chance that you can't see them, they won't see you by the same token.

## Saty Haydrated

Street laborers are inclined to exhaust and heatstroke. Black-top assimilates $95 \%$ of the sun's beams and the black-top temperature effectively increases $30^{\circ} \mathrm{F}$ or more over the encompassing temperature. Laborers ought to drink a lot of water or electrolyte-rich liquids, for example, sports beverages or coconut water. Likewise, avoid the intensity and sun however much as could reasonably be expected, particularly on exceptionally blistering days, to keep away from heat stroke, lack of hydration, and intensity stroke. What other wellbeing tips should street laborers remember? Share your considerations and experiences in the remarks underneath.

## Calculation:

## 3 CASUALTY ACCIDENTS

Table 3-1 : Recorded Casualty Accidents by Division and City

| Division or City | number of accidents ${ }^{1}$ |  |  |  | population ${ }^{2}$ | accid | trates |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | severity |  |  | total | $\left.\left.\frac{\text { population }}{} \right\rvert\,{ }^{( } \mathbf{\prime} 000,000\right)$ | (no. per 10,000 pop'n) |  |
|  | fatal | grievous | simple <br> injury |  |  | fatal accidents | $\begin{gathered} \text { fatal + } \\ \text { injury } \\ \text { accidents } \end{gathered}$ |
| Divisions, excluding Cities |  |  |  |  |  |  |  |
| Barisal | 95 | 14 | 2 | 111 | 8.603 | 0.110 | 0.129 |
| Chittagong | 426 | 85 | 42 | 553 | 22.055 | 0.193 | 0.251 |
| Sylhet | 214 | 60 | 16 | 290 | 8.378 | 0.255 | 0.346 |
| Dhaka | 680 | 168 | 37 | 885 | 35.315 | 0.193 | 0.251 |
| Khulna | 111 | 7 | 1 | 119 | 14.525 | 0.076 | 0.082 |
| Rajshahi | 521 | 118 | 23 | 662 | 31.401 | 0.166 | 0.211 |
| Total | 2047 | 452 | 121 | 2620 | 120.278 | 0.170 | 0.218 |
| Cities |  |  |  |  |  |  |  |
| Chittagong City | 61 | 28 | 8 | 97 | 3.397 | 0.180 | 0.286 |
| Dhaka City | 265 | 140 | 9 | 414 | 5.704 | 0.465 | 0.726 |
| Khulna City | 12 | 2 | 4 | 18 | 0.820 | 0.146 | 0.220 |
| Rajshahi City | 39 | 9 | 0 | 48 | 0.407 | 0.959 | 1.180 |
| Total | 377 | 179 | 21 | 577 | 10.327 | 0.365 | 0.559 |
| TOTAL | 2424 | 631 | 142 | 3197 | 130.605 | 0.186 | 0.245 |

Notes: 1. This is the recorded number of accidents involving casualties (fatal and injury). Property damage only accidents are not included.
2. Year 2005 populations are extrapolated from statistics published in the 2000 Statistical Yearbook and the Population Census 2001 Preliminary Report.

Figure 4.1
Figure 4.1 was used to calculate the fatal accident per 10000 population. People per square kilometer in Dhaka city was noted from world bank data. Based on these two values people around R112 was calculated by taking the total length of the R112 road. The value was then converted in 10000's.

Table 4.1:

| Year | fatal |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | accidents | fatal + |  | People |  |  |
|  | per 10000 | injury | People Per | around | People in |  |
|  | population | accidents | $\mathrm{km}^{\wedge} 2$ | R112 | 10,000 | Fatal |


|  |  | per 10,000 <br> population |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.465 | 0.726 | 1278 | 10873.22 | 1.087322 | 5056.049 |
| 2 |  |  |  | 11634.35 | 1.163435 | 5409.973 |
| 3 |  |  |  | 12448.75 | 1.244875 | 5788.671 |
| 4 |  |  |  | 13320.17 | 1.332017 | 6193.878 |
| 5 |  |  |  | 14252.58 | 1.425258 | 6627.449 |
| 6 |  |  |  | 15250.26 | 1.525026 | 7091.37 |
| 7 |  |  |  | 16317.78 | 1.631778 | 7587.766 |
| 8 |  |  |  | 17460.02 | 1.746002 | 8118.91 |
| 9 |  |  |  | 18682.22 | 1.868222 | 8687.234 |
| 10 |  |  |  | 19989.98 | 1.998998 | 9295.34 |
| 11 |  |  |  | 21389.28 | 2.138928 | 9946.014 |
| 12 |  |  |  | 22886.53 | 2.288653 | 10642.23 |
| 13 |  |  |  | 24488.58 | 2.448858 | 11387.19 |
| 14 |  |  |  | 26202.78 | 2.620278 | 12184.29 |
| 15 |  |  |  | 28036.98 | 2.803698 | 13037.2 |
| 16 |  |  |  | 29999.57 | 2.999957 | 13949.8 |
| 17 |  |  |  | 32099.54 | 3.209954 | 14926.29 |
| 18 |  |  |  | 34346.51 | 3.434651 | 15971.12 |
| 19 |  |  |  | 36750.76 | 3.675076 | 17089.1 |
| 20 |  |  |  | 39323.31 | 3.932331 | 18285.34 |
| 21 |  |  |  | 42075.95 | 4.207595 | 19565.31 |
| 22 |  |  |  | 45021.26 | 4.502126 | 20934.89 |
| 23 |  |  |  | 48172.75 | 4.817275 | 22400.33 |
| 24 |  |  |  | 51544.84 | 5.154484 | 23968.35 |
| 25 |  |  |  | 55152.98 | 5.515298 | 25646.14 |
| 26 |  |  |  | 59013.69 | 5.901369 | 27441.37 |
| 27 |  |  |  | 63144.65 | 6.314465 | 29362.26 |
| 28 |  |  |  | 67564.77 | 6.756477 | 31417.62 |


| 29 |  |  |  | 72294.31 | 7.229431 | 33616.85 |
| ---: | :--- | :--- | :--- | ---: | ---: | :---: |
| 30 |  |  |  | 77354.91 | 7.735491 | 35970.03 |
| 31 |  |  |  | 82769.75 | 8.276975 | 38487.94 |
| 32 |  |  |  | 88563.64 | 8.856364 | 41182.09 |
| 33 |  |  |  | 94763.09 | 9.476309 | 44064.84 |
|  |  |  |  |  | Total Cost |  |

The traffic accident data used in this study were collected by the Accident Research Institute (ARI), BUET. This study used the human capital method to estimate the cost of road accidents in Bangladesh. Estimating the cost of a road accident using the human capital approach includes the economic cost of all casualties, as well as the economic cost considering pain, grief and sufferings, resource of cost like damage of road, damage of vehicleas and medical expenditure.

Table : 4.2

## Current Condition:

Table 14: Human Costs

|  | $\left\|\begin{array}{c} \text { per casualty } \\ \text { cost } \end{array}\right\|$ | Fatal RTA |  | Grievous RTA |  | Simple RTA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | no. | cost | no. | cost | no. | cost |
| Fatality | 206451 | 1.7 | 350967 | 0 | 0 | 0 | 0 |
| Grievous | 2530 | 1.4 | 3542 | 1.7 | 4301 | 0 | 0 |
| Simple | 193 | 1.4 | 270 | 2.2 | 424 | 1.5 | 289 |
| Total |  |  | 354779 |  | 4726 |  | 289 |

Table 13: Medical Costs per RTA Casualty

|  | $\left\lvert\, \begin{gathered} \text { per casualty } \\ \text { cost } \end{gathered}\right.$ | Fatal RTA |  | Grievous RTA |  | Simple RTA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | no. | cost | no. | cost | no. | cost |
| Fatality | 100 | 1.7 | 170 | 0 | 0 | 0 | 0 |
| Grievous | 4200 | 1.4 | 5880 | 1.7 | 7140 | 0 | 0 |
| Simple | 100 | 1.4 | 140 | 2.2 | 220 | 1.5 | 150 |
| Total |  |  | 6190 |  | 7360 |  | 150 |

Table 15: Vehicle related costs (Taka)

|  | Unit costs |
| :--- | ---: |
| fatal | 70000 |
| grievous | 52500 |
| simple | 35000 |
| pdo | 1750 |

These data's were used to forecast the human cost, medical cost, and vehicle related cost for current and future.

Table 4.3:

| Human Cost | Medical Cost | Vehicle related cost |
| ---: | ---: | ---: |
| 1043826405 | 505604.9 | 353923441.2 |
| 1116894253 | 540997.3 | 378698082.1 |
| 1195076851 | 578867.1 | 405206947.8 |
| 1278732231 | 619387.8 | 433571434.2 |
| 1368243487 | 662744.9 | 463921434.6 |
| 1464020531 | 709137 | 496395935 |
| 1566501968 | 758776.6 | 531143650.4 |
| 1676157106 | 811891 | 568323706 |
| 1793488103 | 868723.4 | 608106365.4 |
| 1919032271 | 929534 | 650673811 |
| 2053364530 | 994601.4 | 696220977.7 |
| 2197100047 | 1064223 | 744956446.2 |
| 2350897050 | 1138719 | 797103397.4 |
| 2515459843 | 1218429 | 852900635.2 |
| 2691542033 | 1303720 | 912603679.7 |
| 2879949975 | 1394980 | 976485937.3 |
| 3081546473 | 1492629 | 1044839953 |
| 3297254726 | 1597112 | 1117978750 |
|  |  |  |


| 3528062557 | 1708910 | 1196237262 |
| ---: | ---: | ---: |
| 3775026936 | 1828534 | 1279973870 |
| 4039278821 | 1956531 | 1369572041 |
| 4322028339 | 2093489 | 1465442084 |
| 4624570323 | 2240033 | 1568023030 |
| 4948290245 | 2396835 | 1677784642 |
| 5294670562 | 2564614 | 1795229567 |
| 5665297502 | 2744137 | 1920895637 |
| 6061868327 | 2936226 | 2055358331 |
| 6486199110 | 3141762 | 2199233415 |
| 6940233048 | 3361685 | 2353179754 |
| 7426049361 | 3597003 | 2517902336 |
| 7945872816 | 3848794 | 2694155500 |
| 8502083913 | 4118209 | 2882746385 |
| 9097229787 | 4406484 | 3084538632 |

Table 2: We calculated 3 types of cost for the road Human Cost, Medical Cost and Vehicle related cost. The total cost for Human Cost, Medical Cost and Vehicle related cost was found to be 166299309926.20 in the current condition.

Table: 4.4

Four Lane Condition:

| Human Cost | Medical Cost | Vehicle related cost |
| :---: | :---: | :---: |
| 521913202.6 | 252802.5 | 176961720.6 |
| 558447126.7 | 270498.6 | 189349041 |
| 597538425.6 | 289433.5 | 202603473.9 |
| 639366115.4 | 309693.9 | 216785717.1 |
| 684121743.5 | 331372.5 | 231960717.3 |
| 732010265.5 | 354568.5 | 248197967.5 |
| 783250984.1 | 379388.3 | 265571825.2 |
| 838078553 | 405945.5 | 284161853 |
| 896744051.7 | 434361.7 | 304053182.7 |
| 959516135.3 | 464767 | 325336905.5 |
| 1026682265 | 497300.7 | 348110488.9 |
| 1098550023 | 532111.7 | 372478223.1 |
| 1175448525 | 569359.6 | 398551698.7 |
| 1257729922 | 609214.7 | 426450317.6 |
| 1345771016 | 651859.8 | 456301839.8 |
| 1439974987 | 697490 | 488242968.6 |
| 1540773237 | 746314.3 | 522419976.4 |
| 1648627363 | 798556.2 | 558989374.8 |
| 1764031278 | 854455.2 | 598118631 |
| 1887513468 | 914267.1 | 639986935.2 |
| 2019639411 | 978265.7 | 684786020.7 |
| 2161014169 | 1046744 | 732721042.1 |
| 2312285161 | 1120016 | 784011515.1 |
| 2474145123 | 1198418 | 838892321.1 |
| 2647335281 | 1282307 | 897614783.6 |
| 2832648751 | 1372068 | 960447818.4 |
| 3030934163 | 1468113 | 1027679166 |
| 3243099555 | 1570881 | 1099616707 |


| 3470116524 | 1680843 | 1176589877 |  |  |
| :--- | :--- | :--- | :---: | :---: |
| 3713024680 | 1798502 | 1258951168 |  |  |
| 3972936408 | 1924397 | 1347077750 |  |  |
| 4251041957 | 2059105 | 1441373192 |  |  |
| 4548614894 | 2203242 | 1542269316 |  |  |
|  |  |  |  |  |
| $\mathbf{8 3 1 4 9 6 5 4 9 6 3}$ |  |  |  |  |

Benefit: 83149654963.10

In this we calculated the cost for improvement of the road or for the 4 lane condition of the road, in that case we got the total cost as 83149654963 Which is lower than the current condition, calculating which stands that we will save. After improved the road we got Benifite cost 83149654963.10.

## Chapter 5

## Air Quality Impact

An air pollutant is a gas, liquid droplet, or solid particle that, when released into the atmosphere in high enough concentrations, endangers the health of people, animals, property, and the environment. For millions of urban dwellers throughout the world, air pollution-an obvious environmental side consequence of transportation - has become a health concern (TRB, 1997). Transportation is one of the main causes of air pollution, especially the usage of motor vehicles, which are also the main source of excess regional photochemical oxidant concentrations and a key contributor to local carbon monoxide issues. Typical emissions from transportation vehicles include poisonous gases including carbon monoxide, nitrogen oxides, tiny particulate matter, and others that can be harmful when inhaled. Additionally, rivers, lakes, and forests are negatively impacted by air pollution. As anthropogenic effects on the higher atmosphere grow more obvious, there is still much worry about the role that transportation vehicle use plays in contributing to global warming. For instance, airports are a significant local source of ambient CO breaches and a regional contributor to photochemical oxidant issues. Except in situations where the source of rail energy generation is connected with major pollution, such as coal-based electrical power generation, rail travel is normally not associated with significant air pollution in the modern period.

## Pollutant Types and Sources:

Carbon monoxide, hydrocarbons, sulfur oxides, nitrogen oxides, and particulate matter are examples of primary air pollutants that are released directly into the atmosphere. Secondary air pollutants are those that are created in the atmosphere as a result of physical and chemical processes (such as hydrolysis, oxidation, and photochemistry) on primary pollutants. Examples of secondary air pollutants include ozone and acidic depositions. Carbon dioxide and other greenhouse gases are examples of direct emissions. Forest fires and volcanic eruptions are examples of natural sources of air pollution, while power plants, fuel use, slash-and-burn farming methods, and transportation are examples of artificial sources.Vehicles are the source of three main pollutants:

- One in particular is SOX, a combination of solid particles and liquid droplets that is found in the air and contributes to atmospheric haze that can harm our lungs.
- Carbon monoxide (CO) When fuel is consumed in cars, carbon monoxide is released; breathing air with a high CO 2 concentration can harm vital organs like the heart. According to a poll, cars account for $95 \%$ of all carbon monoxide.
- Nitrogen dioxide (NO2) is produced when fuel burns because of a reaction between nitrogen and oxygen. Nitrogen dioxide is created as a result of vehicles and other


## ESTIMATING POLLUTANT EMISSIONS:

- Emission: Pollutants are being released into the atmosphere in this manner. The quantity of emitting sources, the variety of source types, the kind and extent of activity at the polluting source, and the emission characteristics all affect the overall amount of emissions. For instance, at higher elevations, more pollutants are released by moving automobiles as a result of inefficient combustion brought on by thin air.
- Mobile emission: A motorized vehicle is an example of a movable source of air pollution because it has the ability to move from one location to another. Mobile emissions are those produced by moving sources. The ambient concentration of pollutants released by fixed and mobile sources is used to calculate the overall air quality in a given location.
- Emissions factors: In terms of activity levels like VMT (vehicle miles traveled) or VHT (vehicle hours traveled) for motor vehicles, an emission factor is an average estimate of the rate at which a pollutant is emitted into the atmosphere as a result of some activity (such as motor vehicle operating).


## Method of Estimation :

From the following equation, we can calculate emission the factor and pollution quantity from particular

- A or $\mathrm{VKT}=(\mathrm{L} x \mathrm{AADT})$
- Where,
- $\mathrm{A}=$ Activity level for each pollutant source for each grid ( $\mathrm{km} /$ day )
- $\mathrm{VKT}=$ Vehicle Kilometers Traveled (km/day).
- $\mathrm{L}=$ Road length (km)
- AADT =Annual Average Daily Traffic (traffic volume/day)
- After calculating the vehicle Kilometer Traveled we will use it on total emission calculation.
- Total emission has been calculated as follows:
- $£$ Emission $=($ Zi Ek EFij $\times$ Aik $)$
- Where,
- $i=$ Type of a pollutant
- $j=$ Emission sector like traffic, brick kilns
- $\mathrm{k}=$ Grid cell
- Emission $\mathrm{i}=$ Emissions of pollutant i
- $\mathrm{EF}=$ Emission Factor for each pollutant sector
- $\mathrm{A}=$ Activity level for each pollutant sector

The calculation of emission amounts is dependent on numerous factors and secondary data
it is easy to encounter Uncertainties. That's why we assumed a wide range of values to calculate as much as possible to be done accurately.

## Emission Calculation :

## Table 5.1 :Emission Factors

| Vehicle type | SOx | NOx | CO | PM2.5 | PM10 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Car | 0.40 | 2.77 | 7.30 | 0.84 | 0.84 |
| CNG | 0.20 | 2.77 | 5.00 | 1.50 | 0.75 |
| Motor Cycle | 0.02 | 0.31 | 6.5 | 0.23 | 0.23 |
| Bus | 1.75 | 19.0 | 5.5 | 3.0 | 3.0 |


| Trucks | 0.80 | 9.50 | 5.5 | 3.0 | 1.50 |
| :--- | :--- | :--- | :--- | :--- | :--- |

Table 5.2: Transportation mode with VKT

| Vehicle type | AADT | Road length (km) | VKT (km/day) |
| :--- | :--- | :--- | :--- |
| Car | 2919 | 8.508 | 35903 |
| CNG | 276 |  | 3395 |
| Motor Cycle | 1912 |  | 23517 |
| Bus | 85 |  | 1046 |
| Trucks | 7068 |  | 86936 |
|  | Total | $\mathbf{1 5 0 7 9 7}$ |  |

Table 5.3: Emission for this study area

| Vehicle type | Emission (gm/day) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | SOx | NOx | CO | PM2.5 | PM10 |
| Car | 14361 | 99451 | 262092 | 30159 | 30159 |
| CNG | 679 | 9404 | 16975 | 5093 | 2546 |
| Motor Cycle | 470 | 7290 | 152860 | 5409 | 5409 |
| Bus | 1831 | 19874 | 5753 | 3138 | 3138 |
| Trucks | 69549 | 825892 | 478148 | 260808 | 130404 |
| total | $\mathbf{8 6 8 9 0}$ | $\mathbf{9 6 1 9 1 1}$ | $\mathbf{9 1 5 8 2 8}$ | $\mathbf{3 0 4 6 0 7}$ | $\mathbf{1 7 1 6 5 6}$ |

Table 5.4: Total VKT for 20 years

| Number of vehicles | Road length (km) | Total VKT (km in 20 year) |
| :--- | :--- | :--- |
| 15223 | 8.508 | 2590346 |

Table 5.5 :Taken Maximum emission factor for 20 year

| SOx | NOx | CO | PM2.5 | PM10 |
| :--- | :--- | :--- | :--- | :--- |


| 1.75 | 19.0 | 7.30 | 3.0 | 3.0 |
| :--- | :--- | :--- | :--- | :--- |

Table 5.6 : Emission for this study Area for 20 years

| Component | Emission factor | Total VKT (km in 20 <br> year) | Emissions <br> (ton in year) |
| :---: | :---: | :---: | :---: |
| SOx | 1.75 |  | 4.533 |
| NOx | 19.0 | 2590346 | 49.21 |
|  | 7.30 |  | 19.00 |
| CO | 3.0 |  | 7.80 |
| PM2.5 | 3.0 |  | 7.80 |
| PM10 |  |  |  |

Table 5.7:

| IRI | Fuel per km | Fuel unit rate <br> $($ taka/litre $)$ | Cost for 1 <br> km | VKT (km in <br> 20 years $)$ | Total Fuel Cost |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 8 | 0.08 | 130 | 10.4 | 2590346 | 26939598.4 |
| 3 | -0.27 | 130 | 8.02 | 2590346 | 18372056.2 |

As the emission occurs by burning the fuel, so total fuel cost for 20 years had been calculated. The total fuel cost found to be 26939598.4 BDT if the existing road is left unchanged.

In case of the widening, the IRI will become 3 . Then cost for 1 km will become $22 \%$ less than the previous cost. As a result, the total fuel cost will become 18372056.2.

Total benefit $=26939598.4-18372056.2=8567542.15$ BDT .

## Conclusion:

Air pollution is still mostly caused by transportation, particularly the highway mode. It contributes to global warming, which has negative repercussions not only on a local and regional scale but also on a worldwide one. The dangers of air pollution to human health are well known. It is widely acknowledged that vehicle emissions are the primary factor in both air pollution and health issues. Industrialized nations have been at the forefront of efforts to reduce automotive air pollution through a number of strategies, such as legislation and enforcement, vehicle engine standards, encouraging the use of less polluting modes of transportation, better fuel quality, the use of alternative fuels, and transportation planning and traffic management.


Figure : Air pollution created by vehicles

Appendix:

Table D.1: Emission Factor (gm/km) of SOx

|  | \% | The World Bank | $\frac{m}{2}$ | 霆 | $\sum_{0}^{e}$ | - | 을 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LDV | Gasoline | 0.08 |  |  | 0.05 |  |  |
|  | CNG |  | 0.00 |  |  |  |  |
|  | Disel | 0.40 | 0.30 |  |  |  |  |
| Taxis | CNG | 0.00 |  | 0.10 |  |  |  |
|  | Gasoline |  |  | 0.12 |  |  | 0.13 |
|  | Disel |  |  | 0.50 |  |  |  |
| Car/Jeep/Microbus/St.Wagon | CNG |  | 0.00 | 0.08 |  |  |  |
|  | Gasoline |  | 0.07 | 0.08 |  |  | 0.13 |
|  | CNG |  |  |  |  |  |  |
|  | Disel |  | 0.40 | 0.29 |  | 0.41 | 0.38 |
| Autorickshaw/3W | CNG | 0.00 | 0.00 |  |  | 0.20 |  |
|  | Gasoline |  | 0.02 |  | 0.03 |  |  |
| Tem poo | Gasoline |  |  |  |  |  | 0.05 |
|  | Disel |  |  |  |  |  | 0.39 |
| Bus | CNG | 0.80 | 0.00 |  | 0.40 |  |  |
|  | Disel |  | 1.00 |  |  | 3.14 | 1.75 |
| Minibus | Disel |  |  |  |  | 1.08 | 0.39 |
| Trucks |  | 0.80 |  |  | 1.13 | 4.27 | 1.75 |
| HDT | Disel |  | 1.00 |  |  |  |  |
| Motorcycle/2w | 2-stroke | 0.02 |  |  | 0.19 |  | 0.02 |
|  | 4-stroke |  |  |  |  | 0.22 |  |

Table D．2：Emission Factor（gm／km）of NOx

| ， | \＃ |  | $\stackrel{n}{2}$ | 交 |  |  | \％ | ¢ | 咢 | 会 | 㜢 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Engine Category |  |  |  |  |  |  |
| LDV | Gasoline | 1.50 |  |  |  |  | 1.57 | 2.70 |  |  |  |
|  | Disel | 8.50 | 2.00 |  |  |  |  |  |  |  | 3.15 |
|  | CNG |  | 3.50 |  |  |  |  |  |  |  |  |
| Taxis | Gasoline |  |  | 1.00 | Fumi | 0.50 |  |  |  | 2.70 |  |
|  | CNG | 1.50 |  | 0.80 | Fumi | 1.65 |  |  |  |  |  |
|  | Disel |  |  | 1.50 |  | 1.05 |  |  |  | 1.40 |  |
| Car／Jeep／Microbus／St．Wagon | Gasoline |  | 0.20 | 0.98 | Fumi | 0.50 |  |  |  | 2.70 | 1.80 |
|  | CNG |  | 0.20 | 0.79 | Fumi | 1.65 |  |  |  |  | 2.10 |
|  | Disel |  | 1.25 | 1.47 |  | 0.50 |  | 1.48 |  |  | 2.77 |
| Pick－Up | Gasoline |  |  |  |  | 0.50 |  |  |  |  |  |
|  | NGV＿Gasoline |  |  |  | Fumi | 0.50 |  |  |  |  |  |
|  | NGV＿Disel |  |  |  | DDF | 0.61 |  |  |  |  |  |
|  | Disel |  |  |  |  | 0.50 |  |  |  |  |  |
| Van | Gasoline |  |  |  |  | 0.50 |  |  |  |  |  |
|  | NGV＿Gasoline |  |  |  |  | 5，3 |  |  |  |  |  |
|  | NGV＿Disel |  |  |  |  | 0.91 |  |  |  |  |  |
|  | Disel |  |  |  |  | 1.05 |  |  |  |  |  |
| Autorickshaws $/ 3 \mathrm{~W}$ | Gasoline |  | 0.10 |  |  |  |  |  |  |  | 0.05 |
|  | CNG | 1.50 | 0.35 |  |  |  |  |  |  |  |  |
|  | Disel |  |  |  |  |  | 0.03 | 0.13 |  |  | 2.77 |
| Tem poo | Gasoline |  |  |  |  |  |  |  |  | 0.20 |  |
|  | Disel |  |  |  |  |  |  |  |  | 13.00 |  |
| Buses | CNG | 17.00 | 2.50 |  |  |  | 2.50 |  |  |  | 5.70 |
|  | Disel |  | 10.00 |  |  |  |  | 22.5 |  | 13.00 | 19 |
| Minibus | Disel |  |  |  |  |  |  | 7.55 |  | 13.00 |  |
| Trucks | Disel | 17.00 |  |  |  | 8.83 | 6.48 | 22 | 22 | 13.00 | 9.50 |
| HDT | Disel |  | 10.00 |  |  |  |  |  |  |  |  |
| Motorcycle／2w | 2－stroke | 0.30 | 0.15 |  |  |  | 0.02 | 0.11 |  | 0.07 | 0.03 |
|  | 4－stroke |  |  |  |  |  |  |  |  |  | 0.31 |

Table D.3: Emission Factor (gm/km) of CO


Table D.4: Emission Factor (gm/km) of PM2.5

|  | ¢ | $\frac{n}{2}$ |  |
| :---: | :---: | :---: | :---: |
| LDV | CNG | 0.01 |  |
|  | Disel | 0.50 | 0.80 |
| Car | Gasoline | 0.03 | 0.06 |
|  | CNG | 0.20 | 0.01 |
|  | Disel | 0.60 | 0.84 |
| Three wheels | CNG | 0.05 |  |
|  | Disel |  | 1.50 |
|  | Gasoline | 0.08 | 0.35 |
| Buses | CNG | 0.01 | 0.01 |
|  | Disel | 0.80 | 3.00 |
| HDT | Disel | 1.00 | 1.50 |
| Two wheels | 2-stroke | 0.05 | 0.23 |
|  | 4-stroke |  | 0.07 |

Table D．5：Emission Factor（gm／km）of PM10

| － | ¢ | 弟 号 0 0 0 | $\frac{5}{2}$ | $\begin{aligned} & \text { 菩 } \\ & \sum_{n}^{3} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 量 曲 } \\ & \text { 品 } \end{aligned}$ |  | $\sum_{8}^{0}$ | N | － | $\stackrel{\text { B }}{\text { ¢ }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Engine Category |  |  |  |  |  |  |
| LDV | Gasoline | 0.10 |  |  |  |  | － | 0.06 |  |  | 0.04 |
|  | CNG |  | 0.02 |  |  |  |  |  |  |  |  |
|  | Disel | 0.80 | 1.25 |  |  |  |  |  |  |  | 0.80 |
| Taxis | CNG | 0.03 |  | 0.10 |  |  |  | 0.01 |  |  | 0.01 |
|  | Gasoline |  |  | 0.35 |  |  |  |  |  | 0.20 |  |
|  | Disel |  |  | 0.90 |  | 0.20 |  | 0.84 |  |  | 0.84 |
| Car／Jeep／Microbus／St．Wagon | Gasoline | 0.10 | 0.10 | 0.39 |  |  |  |  | 0.18 | 0.20 | 0.06 |
|  | CNG | 0.03 | 0.05 | 0.20 |  |  |  |  |  |  | 0.01 |
|  | Disel | 0.80 | 1.00 | 0.93 |  | 0.16 |  |  |  | 0.90 | 0.84 |
| Pick－Up | Gasoline |  |  |  |  |  |  |  |  |  |  |
|  | NGV Gasoline |  |  |  |  |  |  |  |  |  |  |
|  | NGV Disel |  |  |  | DDF | 0.08 |  |  |  |  |  |
|  | Disel |  |  |  |  | 0.16 |  |  |  |  |  |
| Van | Gasoline |  |  |  |  |  |  |  |  |  |  |
|  | NGV Gasoline |  |  |  | MPI | 0.00 |  |  |  |  |  |
|  | NGV Disel |  |  |  | DDF | 0.20 |  |  |  |  |  |
|  | Disel |  |  |  |  | 0.20 |  |  |  |  |  |
| Autorickshaw／3W | CNG | 0.03 | 0.10 | 0.10 |  |  |  |  | 0.75 |  |  |
|  | Gasoline |  | 0.20 | 0.20 |  |  |  |  |  |  | 0.35 |
|  | Disel |  |  |  |  |  | 0.75 | 0.50 |  |  | 0.04 |
| Tem poo | Gasoline |  |  |  |  |  |  |  |  | 0.21 |  |
|  | Disel |  |  |  |  |  |  |  |  | 1.50 |  |
| Buses | CNG | 1.60 | 0.02 |  |  |  | 0.10 |  |  |  | 0.01 |
|  | Disel |  | 1.50 |  |  |  |  | 2.00 |  | 3.00 | 3.00 |
| Minibus |  |  |  |  |  |  |  |  | 0.10 | 1.50 |  |
| Trucks | Disel | 1.60 |  | 2.50 |  | 0.66 | 0.45 | 2.00 | 0.45 | 3.00 | 1.50 |
| HDT | Disel |  | 2.00 |  |  |  |  |  |  |  |  |
| Motorcycle／2w | Gasoline | 0.10 | 0.10 | 0.10 |  |  | 0.75 |  | 0.05 | 0.50 | 0．23 |

## Chapter 6

## Noise Impact

Noise has become one of the major defects of road vehicle. When a vehicle runs on a pavement, it creates sound mainly through the engine and the friction of the tire. These noise have health impacts on people living near the roads.

Table 1: Valuation of AMI impacts of noise

| Volume | Additional <br> Lisk of AMI | Health value | Cost per household per dB change <br> (amenity/annoyance <br> costs only ${ }^{33}$ ) |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Current value change in <br> costs (from <br> inclusion of <br> health costs) |  |  |
| $55-60 \mathrm{~dB}$ | $0.00010 \%$ | $£ 2.70$ | $£ 40.00$ | $+6.75 \%$ |
| $60-65 \mathrm{~dB}$ | $0.00168 \%$ | $£ 10.47$ | $£ 53.20$ | $+19.68 \%$ |
| $65-70 \mathrm{~dB}$ | $0.00336 \%$ | $£ 15.71$ | $£ 66.40$ | $+29.29 \%$ |
| $70-75 \mathrm{~dB}$ | $0.00504 \%$ | $£ 29.62$ | $£ 79.60$ | $+37.21 \%$ |
| $75-80 \mathrm{~dB}$ | $0.00720 \%$ | $£ 41.01$ | $£ 92.80$ | $+44.19 \%$ |
| $80-85 \mathrm{~dB}$ | $0.039 \%$ | $£ 53.60$ | $£ 98.00$ | $+54.7 \%$ |

Note: Mid-point marginal values are used for each volume range.

According to this figure, the health value is set in a monetary unit. In the picture, the highest volum level considered is $80-85 \mathrm{~dB}$. Even though Dhaka city junctions usually create more noises.

Table 6. Traffic sound in the Main Road of Dhaka (peak \& off peak hours)

| S.L. | Location | No Of <br> Observations |  | Sound Pressure Levels, dB |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Peak Hours | Off Peak Hours |  |  |
|  |  | Min. | Max. | Min. | Max. |  |
| 01 | Jahangir Gate | 10 | 78.0 | 120.2 | 54.2 | 90.5 |
| 02 | Bangladesh Air <br> Force Officers' Mess | 20 | 71.2 | 112.5 | 50.6 | 84.4 |
| 03 | Awlad Hossain <br> Market | 20 | 73.5 | 110.5 | 48.6 | 81.2 |
| 04 | Farmgate Bus Stop | 25 | 72.6 | 109.9 | 48.2 | 80.6 |
| 05 | Bijoy Sarani |  |  | 88.5 |  |  |

The picture shows, the busy roads of Dhaka city and their produced sound pressure level, dB . During peak hour, the sound pressure level is around 110 or more. However, Rampura Banasree road has fewer vehicle, congestion and noise than these major junctions. So, to work with the data collected through internet to set the noise impact into monetary unit, it is safe to consider 85 dB.

The monetary unit was converted to BDT with the rate of 2010 and then it was converted into present value. Later, the current density of Dhaka city was noted from the world health bank. The density multiplied by 8.508 , the total population living close to the R 112 road was estimated. It was assumed that each family has four members on average. So, the total population was divided by 4 to get the number of the households. Finally multiplying the household number by the health value, the total health value for current condition was calculated.

Founding on air impact and considering the fact that the congestion will be very less in multilane system as the LOS becomes A, the noise reduction is estimated to be $30 \%$ less than the current condition.

Thus the benefit was calculated.
Table 6.1:

| Volume dB | Health value in 2010 | Current <br> Health <br> value | people per <br> km^2 | people <br> around <br> R112 | Total household | Total health value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 85 | 3958.896 | 5025.027 | 1278 | 10873.22 | 2718.306 | 13659560.2 |
|  |  |  |  | 11634.35 | 2908.587 | 14615729.4 |
|  |  |  |  | 12448.75 | 3112.189 | 15638830.5 |
|  |  |  |  | 13320.17 | 3330.042 | 16733548.6 |
|  |  |  |  | 14252.58 | 3563.145 | 17904897 |
|  |  |  |  | 15250.26 | 3812.565 | 19158239.8 |
|  |  |  |  | 16317.78 | 4079.444 | 20499316.6 |
|  |  |  |  | 17460.02 | 4365.005 | 21934268.8 |
|  |  |  |  | 18682.22 | 4670.556 | 23469667.6 |
|  |  |  |  | 19989.98 | 4997.495 | 25112544.3 |
|  |  |  |  | 21389.28 | 5347.319 | 26870422.4 |
|  |  |  |  | 22886.53 | 5721.632 | 28751352 |
|  |  |  |  | 24488.58 | 6122.146 | 30763946.6 |
|  |  |  |  | 26202.78 | 6550.696 | 32917422.9 |
|  |  |  |  | 28036.98 | 7009.245 | 35221642.5 |
|  |  |  |  | 29999.57 | 7499.892 | 37687157.4 |
|  |  |  |  | 32099.54 | 8024.884 | 40325258.5 |
|  |  |  |  | 34346.51 | 8586.626 | 43148026.6 |
|  |  |  |  | 36750.76 | 9187.69 | 46168388.4 |
|  |  |  |  | 39323.31 | 9830.828 | 49400175.6 |
|  |  |  |  | 42075.95 | 10518.99 | 52858187.9 |
|  |  |  |  | 45021.26 | 11255.32 | 56558261.1 |
|  |  |  |  | 48172.75 | 12043.19 | 60517339.3 |
|  |  |  |  | 51544.84 | 12886.21 | 64753553.1 |
|  |  |  |  | 55152.98 | 13788.25 | 69286301.8 |
|  |  |  |  | 59013.69 | 14753.42 | 74136342.9 |
|  |  |  |  | 63144.65 | 15786.16 | 79325886.9 |


|  |  |  |  | 67564.77 | 16891.19 | 84878699 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  | 72294.31 | 18073.58 | 90820208 |
|  |  |  |  | 77354.91 | 19338.73 | 97177622.5 |
|  |  |  |  | 82769.75 | 20692.44 | 103980056 |
|  |  |  | 88563.64 | 22140.91 | 111258660 |  |
|  |  |  | 94763.09 | 23690.77 | 119046766 |  |
| 30\% reduction in multilane system |  |  | Total Cost | 1624578280 |  |  |
| Benefit |  |  | Total Cost | 1137204796 |  |  |

## Chapter 7

## Travel time cost

Travel time cost is very important in road construction costing. It is also known as value of time. This time could be used in an alternative activity which has the potential to produce significant 'utility' known as 'benefit'. If the alternative activity can have a monetary value assigned to it, this can be used as a part of Road construction in the economic appraisal of projects, particularly of the transport projects having relation with consumption of time in the use of their output.

Table 2. Level of services corresponding to delay at the intersection (Highway Capacity Manual, 2010)

| Level of service | The average delay (seconds per vehicle) |
| :---: | :---: |
| A | Less than 10 |
| B | $10-20$ |
| C | $20-35$ |
| D | $35-55$ |
| E | $55-85$ |
| F | More than 80 |

This table was used to calculate the delay time extension for each hour.

| Total Intersection | LOS | Delay | Hour increase |
| :--- | :--- | :--- | :--- |
| 20 | A | 10 | 3.333333333 |
|  | B | 15 | 5 |
|  | C | 25 | 8.333333333 |
|  | D | 45 | 15 |
|  | E | 70 | 23.33333333 |
|  | F | 80 | 26.66666667 |

From the above chart we can see how time increases over the time

Now we will show travel time costs of vehicles.

| Catergory | Occupancy | TTC Per Passenger <br> $(\mathrm{Tk} / \mathrm{hr})$ | TTC per vehicle <br> $(\mathrm{Tk} / \mathrm{Hr})$ |
| :--- | :--- | :--- | :--- |
| Ordinary L Bus | 47 | 49 | 2280 |


| Mini Bus | 35 | 52 | 1803 |
| :--- | :--- | :--- | :--- |
| Microbus | 7 | 107 | 749 |
| Car | 3 | 130 | 390 |
| Auto Rickshaw | 5 | 66 | 328 |
| Motorcycle | 1 | 86 | 86 |


| Category | Number of vehicle | TTC of total <br> passenger | TTC of total vehicle |
| :--- | :--- | :--- | :--- |
| Ordinary L Bus | 85 | 195755 | 193800 |
| Mini Bus | 1199 | 2182180 | 2161797 |
| Microbus | 1764 | 1321236 | 1321236 |
| Car | 2916 | 1137240 | 1137240 |
| Auto Rickshaw | 1767 | 583110 | 579576 |
| Motorcycle | 1912 | 164432 | 164432 |


| category |  | TTC per passenger( tk/ hr) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ordinary <br> L Bus | 47 | 51.45 | $\begin{aligned} & 53.083333 \\ & 33 \end{aligned}$ | $\begin{aligned} & 55.805555 \\ & 56 \end{aligned}$ | 61.25 | $\begin{aligned} & 68.055555 \\ & 56 \end{aligned}$ | $\begin{aligned} & 70.777777 \\ & 78 \end{aligned}$ |
| Mini Bus | 35 | 54.6 | $\begin{aligned} & 56.333333 \\ & 33 \end{aligned}$ | $\begin{aligned} & 59.222222 \\ & 22 \end{aligned}$ | 65 | $\begin{aligned} & 72.222222 \\ & 22 \end{aligned}$ | $\begin{aligned} & 75.111111 \\ & 11 \end{aligned}$ |
| Microbus | 7 | $\begin{aligned} & 112.3 \\ & 5 \end{aligned}$ | $\begin{aligned} & 115.91666 \\ & 67 \end{aligned}$ | $\begin{aligned} & 121.86111 \\ & 11 \end{aligned}$ | $\begin{aligned} & 133.7 \\ & 5 \end{aligned}$ | $\begin{aligned} & 148.61111 \\ & 11 \end{aligned}$ | $\begin{aligned} & 154.55555 \\ & 56 \end{aligned}$ |
| Car | 3 | 136.5 | $\begin{aligned} & 140.83333 \\ & 33 \end{aligned}$ | $\begin{aligned} & 148.05555 \\ & 56 \end{aligned}$ | 162.5 | $\begin{aligned} & 180.55555 \\ & 56 \end{aligned}$ | $\begin{aligned} & 187.77777 \\ & 78 \end{aligned}$ |
| Auto <br> Rickshaw | 5 | 69.3 | 71.5 | $\begin{aligned} & 75.166666 \\ & 67 \end{aligned}$ | 82.5 | $\begin{array}{\|l} \hline 91.666666 \\ 67 \end{array}$ | $\begin{aligned} & 95.333333 \\ & 33 \end{aligned}$ |


| Motorcyc <br> le | 1 | 90.3 | 93.166666 | 97.944444 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 67 | 107.5 | 119.44444 | 124.22222 |  |

Now we will show travel time cost years by years for two lane:

| TTC of Two Lane |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \mathrm{LO} \\ \mathrm{~S} \\ \hline \end{array}$ | $\begin{aligned} & \text { Yea } \\ & \text { r } \end{aligned}$ | Ordinary L <br> Bus | Mini Bus | Micro Bus | Car | Autoricksha w | Motorcycle |
| C | 1 | $\begin{aligned} & 222943.19 \\ & 44 \end{aligned}$ | $\begin{aligned} & 4970521.1 \\ & 11 \end{aligned}$ | 3009482 | 6044220 | 1859473 | $\begin{aligned} & 2621776.8 \\ & 89 \end{aligned}$ |
| C | 2 | $\begin{aligned} & 238549.21 \\ & 81 \end{aligned}$ | $\begin{aligned} & 5318457.5 \\ & 89 \end{aligned}$ | $\begin{aligned} & 3220145.7 \\ & 4 \end{aligned}$ | 6467315.4 | 1989636.11 | $\begin{aligned} & 2805301.2 \\ & 71 \end{aligned}$ |
| C | 3 | $\begin{aligned} & 255247.66 \\ & 33 \end{aligned}$ | $\begin{aligned} & 5690749.6 \\ & 2 \end{aligned}$ | $\begin{aligned} & 3445555.9 \\ & 42 \end{aligned}$ | $\begin{aligned} & \hline 6920027.4 \\ & 78 \\ & \hline \end{aligned}$ | $\begin{array}{\|l} \hline 2128910.63 \\ 8 \end{array}$ | $\begin{aligned} & 3001672.3 \\ & 6 \end{aligned}$ |
| C | 4 | $\begin{aligned} & 273114.99 \\ & 98 \end{aligned}$ | $\begin{aligned} & 6089102.0 \\ & 94 \end{aligned}$ | $\begin{aligned} & 3686744.8 \\ & 58 \end{aligned}$ | $\begin{aligned} & \hline 7404429.4 \\ & 01 \end{aligned}$ | $\begin{aligned} & 2277934.38 \\ & 2 \end{aligned}$ | $\begin{aligned} & 3211789.4 \\ & 25 \end{aligned}$ |
| C | 5 | $\begin{aligned} & 292233.04 \\ & 97 \end{aligned}$ | $\begin{aligned} & 6515339.2 \\ & 4 \end{aligned}$ | $\begin{aligned} & 3944816.9 \\ & 98 \end{aligned}$ | $\begin{aligned} & 7922739.4 \\ & 6 \end{aligned}$ | $\begin{aligned} & 2437389.78 \\ & 9 \end{aligned}$ | $\begin{aligned} & 3436614.6 \\ & 85 \end{aligned}$ |
| C | 6 | $\begin{aligned} & 312689.36 \\ & 32 \end{aligned}$ | $\begin{aligned} & 6971412.9 \\ & 87 \end{aligned}$ | $\begin{aligned} & 4220954.1 \\ & 88 \end{aligned}$ | $\begin{aligned} & 8477331.2 \\ & 22 \end{aligned}$ | $\begin{aligned} & 2608007.07 \\ & 4 \end{aligned}$ | $\begin{aligned} & 3677177.7 \\ & 13 \end{aligned}$ |
| C | 7 | $\begin{aligned} & 334577.61 \\ & 86 \end{aligned}$ | $\begin{aligned} & 7459411.8 \\ & 96 \end{aligned}$ | $\begin{aligned} & 4516420.9 \\ & 81 \end{aligned}$ | $\begin{aligned} & 9070744.4 \\ & 07 \end{aligned}$ | 2790567.57 | $\begin{aligned} & 3934580.1 \\ & 53 \end{aligned}$ |
| D | 8 | $\begin{aligned} & 785849.38 \\ & 23 \end{aligned}$ | $\begin{aligned} & 3679309.4 \\ & 33 \end{aligned}$ | $\begin{aligned} & 2652020.3 \\ & 69 \end{aligned}$ | $\begin{aligned} & 2282698.6 \\ & 58 \end{aligned}$ | $\begin{aligned} & 1170434.04 \\ & 6 \end{aligned}$ | $\begin{aligned} & 330052.32 \\ & 47 \end{aligned}$ |
| D | 9 | $\begin{aligned} & 840858.83 \\ & 91 \end{aligned}$ | $\begin{aligned} & 3936861.0 \\ & 94 \end{aligned}$ | $\begin{aligned} & 2837661.7 \\ & 94 \end{aligned}$ | $\begin{aligned} & 2442487.5 \\ & 64 \end{aligned}$ | $\begin{aligned} & 1252364.42 \\ & 9 \end{aligned}$ | $\begin{aligned} & 353155.98 \\ & 74 \end{aligned}$ |
| D | 10 | $\begin{aligned} & 899718.95 \\ & 78 \end{aligned}$ | $\begin{aligned} & 4212441.3 \\ & 7 \end{aligned}$ | $\begin{aligned} & 3036298.1 \\ & 2 \end{aligned}$ | $\begin{array}{\|l} 2613461.6 \\ 93 \end{array}$ | $\begin{aligned} & 1340029.93 \\ & 9 \end{aligned}$ | $\begin{aligned} & 377876.90 \\ & 65 \end{aligned}$ |
| D | 11 | $\begin{aligned} & 962699.28 \\ & 49 \end{aligned}$ | $\begin{aligned} & 4507312.2 \\ & 66 \end{aligned}$ | $3248838.9$ <br> 88 | $\begin{aligned} & 2796404.0 \\ & 12 \end{aligned}$ | $\begin{aligned} & 1433832.03 \\ & 5 \end{aligned}$ | 404328.29 |


| D | 12 | 1030088.2 <br> 35 | $\begin{aligned} & 4822824.1 \\ & 25 \end{aligned}$ | $3476257.7$ <br> 18 | $\begin{aligned} & 2992152.2 \\ & 93 \end{aligned}$ | $\begin{aligned} & 1534200.27 \\ & 7 \end{aligned}$ | $\begin{aligned} & 432631.27 \\ & 03 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | 13 | $\begin{aligned} & 1102194.4 \\ & 11 \end{aligned}$ | $\begin{array}{\|l} \hline 5160421.8 \\ 14 \end{array}$ | $\begin{aligned} & 3719595.7 \\ & 58 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3201602.9 \\ & 53 \end{aligned}$ | $\begin{aligned} & 1641594.29 \\ & 7 \end{aligned}$ | $\begin{aligned} & 462915.45 \\ & 92 \end{aligned}$ |
| E | 14 | $\begin{aligned} & 1310386.6 \\ & 89 \end{aligned}$ | $\begin{aligned} & 7303771.6 \\ & 15 \end{aligned}$ | $\begin{array}{\|l\|} \hline 4422186.0 \\ 68 \\ \hline \end{array}$ | $\begin{aligned} & 3806350.1 \\ & 78 \end{aligned}$ | 1951673.22 | $\begin{aligned} & 550355.04 \\ & 59 \end{aligned}$ |
| E | 15 | $\begin{array}{\|l} \hline 1402113.7 \\ 57 \end{array}$ | $\begin{array}{\|l} \hline 7815035.6 \\ 28 \end{array}$ | $\begin{array}{\|l\|} \hline 4731739.0 \\ 92 \end{array}$ | $\begin{aligned} & 4072794.6 \\ & 9 \end{aligned}$ | $\begin{aligned} & 2088290.34 \\ & 5 \end{aligned}$ | $\begin{aligned} & 588879.89 \\ & 91 \end{aligned}$ |
| E | 16 | $\begin{aligned} & 1500261.7 \\ & 2 \end{aligned}$ | $\begin{aligned} & 8362088.1 \\ & 22 \end{aligned}$ | $\begin{aligned} & 5062960.8 \\ & 29 \end{aligned}$ | $\begin{aligned} & 4357890.3 \\ & 19 \end{aligned}$ | $\begin{aligned} & 2234470.66 \\ & 9 \end{aligned}$ | $\begin{aligned} & 630101.49 \\ & 21 \end{aligned}$ |
| E | 17 | $\begin{aligned} & 1605280.0 \\ & 41 \end{aligned}$ | $\begin{aligned} & 8947434.2 \\ & 9 \end{aligned}$ | $5417368.0$ $87$ | $\begin{aligned} & 4662942.6 \\ & 41 \end{aligned}$ | $\begin{aligned} & 2390883.61 \\ & 6 \end{aligned}$ | $\begin{aligned} & 674208.59 \\ & 65 \end{aligned}$ |
| E | 18 | $\begin{aligned} & 1717649.6 \\ & 43 \end{aligned}$ | $\begin{aligned} & 9573754.6 \\ & 9 \end{aligned}$ | $\begin{aligned} & \hline 5796583.8 \\ & 53 \end{aligned}$ | $\begin{aligned} & 4989348.6 \\ & 26 \end{aligned}$ | $\begin{aligned} & 2558245.46 \\ & 9 \end{aligned}$ | $\begin{aligned} & 721403.19 \\ & 83 \end{aligned}$ |
| E | 19 | $1837885.1$ <br> 18 | $\begin{aligned} & 10243917 . \\ & 52 \end{aligned}$ | $\begin{aligned} & 6202344.7 \\ & 23 \end{aligned}$ | $\begin{aligned} & 5338603.0 \\ & 3 \end{aligned}$ | $\begin{aligned} & 2737322.65 \\ & 2 \end{aligned}$ | $\begin{aligned} & 771901.42 \\ & 22 \end{aligned}$ |
| F | 20 | $\begin{aligned} & 2045198.5 \\ & 6 \end{aligned}$ | $\begin{aligned} & 11399431 . \\ & 41 \end{aligned}$ | $6901969.2$ <br> 07 | $\begin{aligned} & \hline 5940797.4 \\ & 51 \end{aligned}$ | $\begin{aligned} & 3046092.64 \\ & 7 \end{aligned}$ | $\begin{aligned} & 858971.90 \\ & 26 \end{aligned}$ |
| F | 21 | $\begin{aligned} & \hline 2188362.4 \\ & 59 \end{aligned}$ | $\begin{aligned} & 12197391 . \\ & 61 \end{aligned}$ | $\begin{aligned} & 7385107.0 \\ & 52 \end{aligned}$ | $\begin{aligned} & 6356653.2 \\ & 73 \end{aligned}$ | $\begin{aligned} & 3259319.13 \\ & 2 \end{aligned}$ | $\begin{aligned} & 919099.93 \\ & 58 \end{aligned}$ |
| F | 22 | $\begin{aligned} & 2341547.8 \\ & 31 \end{aligned}$ | $\begin{aligned} & 13051209 . \\ & 03 \end{aligned}$ | $\begin{aligned} & 7902064.5 \\ & 45 \end{aligned}$ | $\begin{aligned} & 6801619.0 \\ & 02 \end{aligned}$ | $3487471.47$ <br> 1 | $\begin{aligned} & 983436.93 \\ & 13 \end{aligned}$ |
| F | 23 | $\begin{aligned} & 2505456.1 \\ & 79 \end{aligned}$ | $\begin{aligned} & 13964793 . \\ & 66 \end{aligned}$ | $\begin{aligned} & 8455209.0 \\ & 64 \end{aligned}$ | $\begin{aligned} & 7277732.3 \\ & 32 \end{aligned}$ | $\begin{aligned} & 3731594.47 \\ & 4 \end{aligned}$ | $\begin{aligned} & 1052277.5 \\ & 16 \end{aligned}$ |
| F | 24 | $\begin{aligned} & 2680838.1 \\ & 12 \end{aligned}$ | $\begin{aligned} & 14942329 . \\ & 21 \end{aligned}$ | $\begin{aligned} & 9047073.6 \\ & 98 \end{aligned}$ | $\begin{aligned} & 7787173.5 \\ & 95 \end{aligned}$ | $\begin{aligned} & 3992806.08 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1125936.9 \\ & 43 \end{aligned}$ |
| F | 25 | $\begin{aligned} & 2868496.7 \\ & 8 \end{aligned}$ | $\begin{aligned} & 15988292 . \\ & 26 \end{aligned}$ | $9680368.8$ <br> 57 | $\begin{aligned} & 8332275.7 \\ & 47 \end{aligned}$ | $\begin{aligned} & 4272302.51 \\ & 4 \end{aligned}$ | $\begin{aligned} & 1204752.5 \\ & 29 \end{aligned}$ |
| F | 26 | $3069291.5$ <br> 54 | $\begin{aligned} & 17107472 . \\ & 72 \end{aligned}$ | $10357994 .$ <br> 68 | $\begin{aligned} & 8915535.0 \\ & 49 \end{aligned}$ | 4571363.69 | $\begin{aligned} & 1289085.2 \\ & 06 \end{aligned}$ |


| F | 27 | $\begin{aligned} & 3284141.9 \\ & 63 \end{aligned}$ | $\begin{aligned} & 18304995 . \\ & 81 \end{aligned}$ | $\begin{aligned} & 11083054 . \\ & 3 \end{aligned}$ | $\begin{aligned} & 9539622.5 \\ & 03 \end{aligned}$ | $\begin{aligned} & 4891359.14 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1379321.1 \\ & 7 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F | 28 | 3514031.9 | $\begin{aligned} & 19586345 . \\ & 51 \end{aligned}$ | $\begin{aligned} & 11858868 . \\ & 11 \end{aligned}$ | $\begin{aligned} & 10207396 . \\ & 08 \end{aligned}$ | $\begin{aligned} & 5233754.28 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1475873.6 \\ & 52 \end{aligned}$ |
| F | 29 | $\begin{aligned} & 3760014.1 \\ & 33 \end{aligned}$ | $\begin{aligned} & \hline 20957389 . \\ & 7 \end{aligned}$ | $\begin{aligned} & 12688988 . \\ & 87 \end{aligned}$ | $\begin{aligned} & 10921913 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 5600117.08 \\ & 9 \end{aligned}$ | $\begin{aligned} & 1579184.8 \\ & 08 \end{aligned}$ |
| F | 30 | $\begin{aligned} & 4023215.1 \\ & 23 \end{aligned}$ | $\begin{aligned} & 22424406 . \\ & 98 \end{aligned}$ | $\begin{aligned} & 13577218 . \\ & 09 \end{aligned}$ | $\begin{aligned} & 11686447 . \\ & 77 \end{aligned}$ | $\begin{aligned} & 5992125.28 \\ & 5 \end{aligned}$ | $\begin{aligned} & 1689727.7 \\ & 44 \end{aligned}$ |
| F | 31 | $\begin{aligned} & 4304840.1 \\ & 81 \end{aligned}$ | $\begin{aligned} & 23994115 . \\ & 47 \end{aligned}$ | $\begin{aligned} & 14527623 . \\ & 36 \end{aligned}$ | $\begin{aligned} & 12504499 . \\ & 11 \end{aligned}$ | $\begin{aligned} & 6411574.05 \\ & 5 \end{aligned}$ | $\begin{aligned} & 1808008.6 \\ & 86 \end{aligned}$ |
| F | 32 | $\begin{aligned} & 4606178.9 \\ & 94 \end{aligned}$ | $\begin{aligned} & 25673703 . \\ & 55 \end{aligned}$ | 15544557 | $\begin{aligned} & 13379814 . \\ & 05 \end{aligned}$ | $\begin{aligned} & 6860384.23 \\ & 9 \end{aligned}$ | $\begin{aligned} & 1934569.2 \\ & 94 \end{aligned}$ |
| F | 33 | $\begin{aligned} & 4928611.5 \\ & 24 \end{aligned}$ | $\begin{aligned} & 27470862 . \\ & 8 \end{aligned}$ | $16632675 .$ <br> 99 | $\begin{aligned} & 14316401 . \\ & 04 \end{aligned}$ | $\begin{aligned} & 7340611.13 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2069989.1 \\ & 45 \end{aligned}$ |
| F | 34 | $\begin{aligned} & 5273614.3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 29393823 . \\ & 2 \end{aligned}$ | $\begin{aligned} & 17796963 . \\ & 3 \end{aligned}$ | $\begin{aligned} & 15318549 . \\ & 11 \end{aligned}$ | $\begin{aligned} & 7854453.91 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2214888.3 \\ & 85 \end{aligned}$ |
| F | 35 | $\begin{aligned} & 5642767.3 \\ & 33 \end{aligned}$ | $\begin{aligned} & 31451390 . \\ & 82 \end{aligned}$ | $\begin{aligned} & 19042750 . \\ & 74 \end{aligned}$ | $\begin{aligned} & 16390847 . \\ & 54 \end{aligned}$ | $\begin{aligned} & 8404265.68 \\ & 9 \end{aligned}$ | $\begin{aligned} & 2369930.5 \\ & 72 \end{aligned}$ |
| F | 36 | $\begin{aligned} & 6037761.0 \\ & 47 \end{aligned}$ | $33652988 .$ <br> 18 | $\begin{aligned} & 20375743 . \\ & 29 \end{aligned}$ | $\begin{aligned} & 17538206 . \\ & 87 \end{aligned}$ | $\begin{aligned} & 8992564.28 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2535825.7 \\ & 12 \end{aligned}$ |
| F | 37 | $\begin{aligned} & 6460404.3 \\ & 2 \end{aligned}$ | $\begin{aligned} & 36008697 . \\ & 35 \end{aligned}$ | $\begin{aligned} & 21802045 . \\ & 32 \end{aligned}$ | $\begin{aligned} & 18765881 . \\ & 35 \end{aligned}$ | $\begin{aligned} & 9622043.78 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2713333.5 \\ & 12 \end{aligned}$ |
| F | 38 | $\begin{aligned} & 6912632.6 \\ & 23 \end{aligned}$ | $38529306 .$ <br> 16 | $\begin{aligned} & 23328188 . \\ & 49 \end{aligned}$ | $\begin{aligned} & 20079493 . \\ & 05 \end{aligned}$ | $\begin{aligned} & 10295586.8 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2903266.8 \\ & 58 \end{aligned}$ |
| F | 39 | $\begin{aligned} & 7396516.9 \\ & 06 \end{aligned}$ | $\begin{aligned} & 41226357 . \\ & 6 \end{aligned}$ | $\begin{aligned} & 24961161 . \\ & 68 \end{aligned}$ | $\begin{aligned} & 21485057 . \\ & 56 \end{aligned}$ | $\begin{aligned} & 11016277.9 \\ & 3 \end{aligned}$ | $\begin{aligned} & 3106495.5 \\ & 38 \end{aligned}$ |
| F | 40 | $\begin{aligned} & 7914273.0 \\ & 9 \end{aligned}$ | $\begin{aligned} & 44112202 . \\ & 63 \end{aligned}$ | 26708443 | $\begin{aligned} & 22989011 . \\ & 59 \end{aligned}$ | $\begin{aligned} & 11787417.3 \\ & 9 \end{aligned}$ | $\begin{aligned} & 3323950.2 \\ & 25 \end{aligned}$ |
| F | 41 | $\begin{aligned} & 8468272.2 \\ & 06 \end{aligned}$ | $\begin{aligned} & 47200056 . \\ & 81 \end{aligned}$ | $\begin{aligned} & 28578034 . \\ & 01 \end{aligned}$ | $\begin{aligned} & 24598242 . \\ & 4 \end{aligned}$ | 12612536.6 | $\begin{aligned} & 3556626.7 \\ & 41 \end{aligned}$ |

$\left.\begin{array}{|l|l|l|l|l|l|l|l|}\hline \text { F } & 42 & \begin{array}{l}9061051.2 \\ 6\end{array} & \begin{array}{l}50504060 . \\ 79\end{array} & \begin{array}{l}30578496 . \\ 39\end{array} & \begin{array}{l}26320119 . \\ 37\end{array} & \begin{array}{l}13495414.1 \\ 7\end{array} & 3805590.6 \\ \hline \text { F } & 43 & 9695324.8 & 54039345 . & 32718991 . & 28162527 . & 14440093.1 & 4071981.9 \\ \hline 04\end{array}\right)$

Now we will show travel time cost years by years for multi lane:

| LO <br> S | Yea <br> r | Ordinary L <br> Bus | Mini Bus | Micro Bus | Car | Autoricksha <br> w | Motorcycle |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| A | 1 | 205542.75 | 2291289 | 1387297.8 | 1194102 | 612265.5 | 172653.6 |
| A | 2 | 219930.74 <br> 25 | 2451679.2 <br> 3 | 1484408.6 <br> 46 | 1277689.1 <br> 4 | 655124.085 | 184739.35 |
| A | 3 | 235325.89 <br> 45 | 2623296.7 <br> 76 | 1588317.2 <br> 51 | 1367127.3 <br> 8 | 700982.771 | 197671.10 |
| A | 4 | 251798.70 <br> 71 | 2806927.5 <br> 5 | 1699499.4 <br> 59 | 1462826.2 <br> 96 | 750051.564 | 211508.08 |
| A | 5 | 269424.61 <br> 66 | 3003412.4 <br> 79 | 1818464.4 <br> 21 | 1565224.1 <br> 37 | 802555.174 | 226313.65 |


| A | 6 | $\begin{aligned} & 288284.33 \\ & 97 \end{aligned}$ | $\begin{aligned} & 3213651.3 \\ & 52 \end{aligned}$ | $\begin{aligned} & 1945756.9 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1674789.8 \\ & 27 \end{aligned}$ | $\begin{aligned} & 858734.036 \\ & 7 \end{aligned}$ | $242155.60$ <br> 55 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 7 | $\begin{aligned} & \hline 308464.24 \\ & 35 \end{aligned}$ | $\begin{aligned} & 3438606.9 \\ & 47 \end{aligned}$ | $\begin{aligned} & 2081959.9 \\ & 16 \end{aligned}$ | $\begin{aligned} & 1792025.1 \\ & 15 \end{aligned}$ | $\begin{aligned} & 918845.419 \\ & 2 \end{aligned}$ | $\begin{aligned} & 259106.49 \\ & 79 \end{aligned}$ |
| A | 8 | $\begin{aligned} & 330056.74 \\ & 06 \end{aligned}$ | $\begin{array}{\|l\|} \hline 3679309.4 \\ 33 \end{array}$ | $2227697.1$ <br> 1 | $\begin{aligned} & 1917466.8 \\ & 73 \end{aligned}$ | $\begin{aligned} & 983164.598 \\ & 6 \end{aligned}$ | $\begin{aligned} & 277243.95 \\ & 27 \end{aligned}$ |
| A | 9 | $\begin{aligned} & 353160.71 \\ & 24 \end{aligned}$ | $\begin{array}{\|l} \hline 3936861.0 \\ 94 \end{array}$ | $\begin{aligned} & 2383635.9 \\ & 07 \end{aligned}$ | $\begin{aligned} & 2051689.5 \\ & 54 \end{aligned}$ | 1051986.12 | $\begin{aligned} & 296651.02 \\ & 94 \end{aligned}$ |
| A | 10 | $\begin{array}{\|l} \hline 377881.96 \\ 23 \end{array}$ | $\begin{array}{\|l} \hline 4212441.3 \\ 7 \end{array}$ | $\begin{aligned} & \hline 2550490.4 \\ & 21 \end{aligned}$ | $\begin{aligned} & 2195307.8 \\ & 22 \end{aligned}$ | $\begin{aligned} & 1125625.14 \\ & 9 \end{aligned}$ | $\begin{aligned} & 317416.60 \\ & 15 \end{aligned}$ |
| A | 11 | $\begin{aligned} & 404333.69 \\ & 96 \end{aligned}$ | $\begin{aligned} & 4507312.2 \\ & 66 \end{aligned}$ | $\begin{aligned} & 2729024.7 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2348979.3 \\ & 7 \end{aligned}$ | $\begin{aligned} & 1204418.90 \\ & 9 \end{aligned}$ | $\begin{aligned} & 339635.76 \\ & 36 \end{aligned}$ |
| B | 12 | $\begin{aligned} & 446371.56 \\ & 84 \end{aligned}$ | $\begin{aligned} & 4975929.6 \\ & 53 \end{aligned}$ | $\begin{aligned} & 3012756.6 \\ & 89 \end{aligned}$ | $\begin{aligned} & 2593198.6 \\ & 54 \end{aligned}$ | 1329640.24 | $374947.10$ <br> 09 |
| B | 13 | $\begin{aligned} & 477617.57 \\ & 82 \end{aligned}$ | $\begin{aligned} & 5324244.7 \\ & 28 \end{aligned}$ | $3223649.6$ <br> 57 | $\begin{aligned} & 2774722.5 \\ & 6 \end{aligned}$ | $\begin{aligned} & 1422715.05 \\ & 7 \end{aligned}$ | $\begin{aligned} & 401193.39 \\ & 8 \end{aligned}$ |
| B | 14 | $\begin{aligned} & 511050.80 \\ & 87 \end{aligned}$ | $\begin{aligned} & 5696941.8 \\ & 59 \end{aligned}$ | $\begin{aligned} & 3449305.1 \\ & 33 \end{aligned}$ | $\begin{aligned} & 2968953.1 \\ & 39 \end{aligned}$ | $\begin{aligned} & 1522305.11 \\ & 1 \end{aligned}$ | $\begin{aligned} & 429276.93 \\ & 58 \end{aligned}$ |
| B | 15 | $\begin{aligned} & 546824.36 \\ & 53 \end{aligned}$ | $\begin{aligned} & 6095727.7 \\ & 9 \end{aligned}$ | $\begin{aligned} & 3690756.4 \\ & 92 \end{aligned}$ | $\begin{aligned} & 3176779.8 \\ & 58 \end{aligned}$ | $\begin{aligned} & 1628866.46 \\ & 9 \end{aligned}$ | $\begin{aligned} & 459326.32 \\ & 13 \end{aligned}$ |
| B | 16 | $\begin{aligned} & 585102.07 \\ & 09 \end{aligned}$ | $\begin{aligned} & 6522428.7 \\ & 35 \end{aligned}$ | $\begin{aligned} & 3949109.4 \\ & 46 \end{aligned}$ | $\begin{aligned} & 3399154.4 \\ & 48 \end{aligned}$ | $\begin{aligned} & 1742887.12 \\ & 2 \end{aligned}$ | $\begin{aligned} & 491479.16 \\ & 38 \end{aligned}$ |
| B | 17 | $\begin{aligned} & 626059.21 \\ & 58 \end{aligned}$ | $\begin{aligned} & 6978998.7 \\ & 46 \end{aligned}$ | $\begin{aligned} & 4225547.1 \\ & 08 \end{aligned}$ | $\begin{aligned} & 3637095.2 \\ & 6 \end{aligned}$ | 1864889.22 | $\begin{aligned} & 525882.70 \\ & 53 \end{aligned}$ |
| B | 18 | $\begin{aligned} & 669883.36 \\ & 09 \end{aligned}$ | $\begin{aligned} & 7467528.6 \\ & 58 \end{aligned}$ | $\begin{aligned} & 4521335.4 \\ & 05 \end{aligned}$ | $\begin{aligned} & 3891691.9 \\ & 28 \end{aligned}$ | $\begin{aligned} & 1995431.46 \\ & 6 \end{aligned}$ | $\begin{aligned} & 562694.49 \\ & 47 \end{aligned}$ |
| C | 19 | $\begin{aligned} & 753532.89 \\ & 86 \end{aligned}$ | $\begin{aligned} & 8400012.3 \\ & 65 \end{aligned}$ | $\begin{aligned} & 5085922.6 \\ & 73 \end{aligned}$ | $\begin{aligned} & 4377654.4 \\ & 84 \end{aligned}$ | $\begin{aligned} & 2244604.57 \\ & 4 \end{aligned}$ | $\begin{aligned} & 632959.16 \\ & 62 \end{aligned}$ |
| C | 20 | $\begin{aligned} & 806280.20 \\ & 15 \end{aligned}$ | $\begin{aligned} & 8988013.2 \\ & 31 \end{aligned}$ | $\begin{aligned} & 5441937.2 \\ & 6 \end{aligned}$ | $\begin{aligned} & 4684090.2 \\ & 98 \end{aligned}$ | $\begin{aligned} & 2401726.89 \\ & 5 \end{aligned}$ | $\begin{aligned} & 677266.30 \\ & 78 \end{aligned}$ |


| C | 21 | $\begin{aligned} & 862719.81 \\ & 56 \end{aligned}$ | $\begin{aligned} & 9617174.1 \\ & 57 \end{aligned}$ | $\begin{aligned} & 5822872.8 \\ & 68 \end{aligned}$ | $\begin{aligned} & 5011976.6 \\ & 19 \end{aligned}$ | $\begin{aligned} & 2569847.77 \\ & 7 \end{aligned}$ | $\begin{aligned} & 724674.94 \\ & 94 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C | 22 | $\begin{aligned} & 923110.20 \\ & 26 \end{aligned}$ | $\begin{aligned} & 10290376 . \\ & 35 \end{aligned}$ | $\begin{array}{\|l\|} \hline 6230473.9 \\ 69 \end{array}$ | $\begin{aligned} & 5362814.9 \\ & 82 \end{aligned}$ | $\begin{array}{\|l} \hline 2749737.12 \\ 2 \end{array}$ | $\begin{aligned} & 775402.19 \\ & 58 \end{aligned}$ |
| C | 23 | $\begin{aligned} & 987727.91 \\ & 68 \end{aligned}$ | $\begin{aligned} & 11010702 . \\ & 69 \end{aligned}$ | $\begin{aligned} & 6666607.1 \\ & 46 \end{aligned}$ | $\begin{aligned} & 5738212.0 \\ & 31 \end{aligned}$ | 2942218.72 | $\begin{aligned} & 829680.34 \\ & 95 \end{aligned}$ |
| C | 24 | $\begin{aligned} & 1056868.8 \\ & 71 \end{aligned}$ | $\begin{aligned} & 11781451 . \\ & 88 \end{aligned}$ | $\begin{aligned} & 7133269.6 \\ & 47 \end{aligned}$ | $\begin{array}{\|l\|} \hline 6139886.8 \\ 73 \\ \hline \end{array}$ | $\begin{array}{\|l} \hline 3148174.03 \\ 1 \end{array}$ | $\begin{aligned} & 887757.97 \\ & 4 \end{aligned}$ |
| D | 25 | $\begin{aligned} & 1241176.4 \\ & 91 \end{aligned}$ | $\begin{aligned} & 13836022 . \\ & 15 \end{aligned}$ | $\begin{aligned} & 8377242.2 \\ & 8 \end{aligned}$ | $\begin{aligned} & 7210623.2 \\ & 43 \end{aligned}$ | $\begin{aligned} & 3697184.86 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1042574.3 \\ & 04 \end{aligned}$ |
| D | 26 | $\begin{aligned} & 1328058.8 \\ & 46 \end{aligned}$ | $\begin{aligned} & 14804543 . \\ & 7 \end{aligned}$ | $\begin{aligned} & 8963649.2 \\ & 4 \end{aligned}$ | $\begin{array}{\|l} \hline 7715366.8 \\ 7 \end{array}$ | $\begin{aligned} & 3955987.80 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1115554.5 \\ & 05 \end{aligned}$ |
| D | 27 | $\begin{aligned} & 1421022.9 \\ & 65 \end{aligned}$ | $\begin{aligned} & 15840861 . \\ & 76 \end{aligned}$ | $\begin{aligned} & 9591104.6 \\ & 86 \end{aligned}$ | $\begin{aligned} & 8255442.5 \\ & 5 \end{aligned}$ | $\begin{array}{\|l} 4232906.95 \\ 5 \end{array}$ | $\begin{aligned} & 1193643.3 \\ & 2 \end{aligned}$ |
| D | 28 | $\begin{aligned} & 1520494.5 \\ & 72 \end{aligned}$ | $\begin{aligned} & 16949722 . \\ & 08 \end{aligned}$ | $\begin{aligned} & 10262482 . \\ & 01 \end{aligned}$ | $\begin{aligned} & 8833323.5 \\ & 29 \end{aligned}$ | $\begin{aligned} & 4529210.44 \\ & 2 \end{aligned}$ | $\begin{aligned} & 1277198.3 \\ & 53 \end{aligned}$ |
| E | 29 | $\begin{aligned} & 1807699.1 \\ & 03 \end{aligned}$ | $\begin{aligned} & 20151336 . \\ & 25 \end{aligned}$ | $\begin{aligned} & 12200950 . \\ & 84 \end{aligned}$ | $\begin{aligned} & 10501840 . \\ & 2 \end{aligned}$ | 5384727.97 | $\begin{aligned} & 1518446.9 \\ & 3 \end{aligned}$ |
| E | 30 | $\begin{aligned} & 1934238.0 \\ & 4 \end{aligned}$ | $\begin{aligned} & 21561929 . \\ & 79 \end{aligned}$ | $\begin{aligned} & 13055017 . \\ & 4 \end{aligned}$ | $\begin{aligned} & 11236969 . \\ & 01 \end{aligned}$ | $\begin{aligned} & 5761658.92 \\ & 8 \end{aligned}$ | $1624738.2$ <br> 15 |
| E | 31 | $\begin{aligned} & 2069634.7 \\ & 03 \end{aligned}$ | $\begin{aligned} & 23071264 . \\ & 87 \end{aligned}$ | $\begin{aligned} & 13968868 . \\ & 62 \end{aligned}$ | $\begin{aligned} & 12023556 . \\ & 84 \end{aligned}$ | $\begin{aligned} & 6164975.05 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1738469.8 \\ & 91 \end{aligned}$ |
| E | 32 | $\begin{aligned} & 2214509.1 \\ & 32 \end{aligned}$ | $\begin{aligned} & 24686253 . \\ & 41 \end{aligned}$ | $\begin{aligned} & 14946689 . \\ & 42 \end{aligned}$ | $\begin{aligned} & 12865205 . \\ & 82 \end{aligned}$ | $\begin{aligned} & 6596523.30 \\ & 6 \end{aligned}$ | $\begin{aligned} & 1860162.7 \\ & 83 \end{aligned}$ |
| F | 33 | $\begin{aligned} & 2464305.7 \\ & 62 \end{aligned}$ | $\begin{aligned} & 27470862 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 16632675 . \\ & 99 \end{aligned}$ | $\begin{aligned} & 14316401 . \\ & 04 \end{aligned}$ | $\begin{array}{\|l} \hline 7340611.13 \\ 5 \end{array}$ | $\begin{aligned} & 2069989.1 \\ & 45 \end{aligned}$ |
| F | 34 | $\begin{aligned} & 2636807.1 \\ & 65 \end{aligned}$ | $\begin{aligned} & 29393823 . \\ & 2 \end{aligned}$ | $\begin{aligned} & 17796963 . \\ & 3 \end{aligned}$ | $15318549 .$ <br> 11 | $\begin{array}{\|l\|} \hline 7854453.91 \\ 5 \end{array}$ | $\begin{aligned} & 2214888.3 \\ & 85 \end{aligned}$ |
| F | 35 | $\begin{aligned} & 2821383.6 \\ & 67 \end{aligned}$ | $\begin{aligned} & 31451390 . \\ & 82 \end{aligned}$ | $\begin{aligned} & 19042750 . \\ & 74 \end{aligned}$ | $\begin{aligned} & 16390847 . \\ & 54 \end{aligned}$ | $\begin{aligned} & 8404265.68 \\ & 9 \end{aligned}$ | $\begin{aligned} & 2369930.5 \\ & 72 \end{aligned}$ |


| F | 36 | $\begin{aligned} & 3018880.5 \\ & 23 \end{aligned}$ | $\begin{aligned} & 33652988 . \\ & 18 \end{aligned}$ | $\begin{aligned} & 20375743 . \\ & 29 \end{aligned}$ | $\begin{aligned} & 17538206 . \\ & 87 \end{aligned}$ | $\begin{aligned} & 8992564.28 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2535825.7 \\ & 12 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F | 37 | $\begin{aligned} & 3230202.1 \\ & 6 \end{aligned}$ | $\begin{aligned} & 36008697 . \\ & 35 \end{aligned}$ | $\begin{aligned} & 21802045 . \\ & 32 \end{aligned}$ | $\begin{aligned} & 18765881 . \\ & 35 \end{aligned}$ | $\begin{aligned} & 9622043.78 \\ & 7 \end{aligned}$ | $\begin{aligned} & 2713333.5 \\ & 12 \end{aligned}$ |
| F | 38 | $\begin{aligned} & 3456316.3 \\ & 11 \end{aligned}$ | $\begin{aligned} & 38529306 . \\ & 16 \end{aligned}$ | $\begin{aligned} & 23328188 . \\ & 49 \end{aligned}$ | $\begin{aligned} & 20079493 . \\ & 05 \end{aligned}$ | $\begin{aligned} & 10295586.8 \\ & 5 \end{aligned}$ | $\begin{aligned} & 2903266.8 \\ & 58 \end{aligned}$ |
| F | 39 | $\begin{aligned} & 3698258.4 \\ & 53 \end{aligned}$ | $\begin{aligned} & 41226357 . \\ & 6 \end{aligned}$ | $\begin{aligned} & 24961161 . \\ & 68 \end{aligned}$ | $\begin{aligned} & 21485057 . \\ & 56 \end{aligned}$ | $\begin{aligned} & 11016277.9 \\ & 3 \end{aligned}$ | $\begin{aligned} & 3106495.5 \\ & 38 \end{aligned}$ |
| F | 40 | $\begin{aligned} & 3957136.5 \\ & 45 \end{aligned}$ | $\begin{aligned} & 44112202 . \\ & 63 \end{aligned}$ | 26708443 | $\begin{aligned} & 22989011 . \\ & 59 \end{aligned}$ | $\begin{aligned} & 11787417.3 \\ & 9 \end{aligned}$ | $\begin{aligned} & 3323950.2 \\ & 25 \end{aligned}$ |
| F | 41 | $\begin{aligned} & 4234136.1 \\ & 03 \end{aligned}$ | $\begin{aligned} & 47200056 . \\ & 81 \end{aligned}$ | $\begin{aligned} & 28578034 . \\ & 01 \end{aligned}$ | $\begin{aligned} & 24598242 . \\ & 4 \end{aligned}$ | 12612536.6 | $\begin{aligned} & 3556626.7 \\ & 41 \end{aligned}$ |
| F | 42 | $\begin{aligned} & 4530525.6 \\ & 3 \end{aligned}$ | $\begin{aligned} & 50504060 . \\ & 79 \end{aligned}$ | $\begin{aligned} & 30578496 . \\ & 39 \end{aligned}$ | $\begin{aligned} & 26320119 . \\ & 37 \end{aligned}$ | $\begin{aligned} & 13495414.1 \\ & 7 \end{aligned}$ | $\begin{aligned} & 3805590.6 \\ & 13 \end{aligned}$ |
| F | 43 | $\begin{aligned} & 4847662.4 \\ & 24 \end{aligned}$ | $\begin{aligned} & 54039345 . \\ & 04 \end{aligned}$ | $32718991 .$ <br> 14 | $\begin{aligned} & 28162527 . \\ & 73 \end{aligned}$ | $14440093.1$ $6$ | $\begin{aligned} & 4071981.9 \\ & 56 \end{aligned}$ |
| F | 44 | $\begin{aligned} & 5186998.7 \\ & 94 \end{aligned}$ | $\begin{aligned} & 57822099 . \\ & 2 \end{aligned}$ | $\begin{aligned} & 35009320 . \\ & 52 \end{aligned}$ | $\begin{aligned} & 30133904 . \\ & 67 \end{aligned}$ | $\begin{aligned} & 15450899.6 \\ & 8 \end{aligned}$ | $\begin{aligned} & 4357020.6 \\ & 93 \end{aligned}$ |
| F | 45 | $\begin{aligned} & 5550088.7 \\ & 09 \end{aligned}$ | $61869646 .$ <br> 14 | $\begin{aligned} & 37459972 . \\ & 96 \end{aligned}$ | 32243278 | $\begin{aligned} & 16532462.6 \\ & 6 \end{aligned}$ | $\begin{aligned} & 4662012.1 \\ & 41 \end{aligned}$ |
| F | 46 | $\begin{aligned} & 5938594.9 \\ & 19 \end{aligned}$ | $\begin{aligned} & 66200521 . \\ & 37 \end{aligned}$ | $\begin{aligned} & 40082171 . \\ & 06 \end{aligned}$ | $\begin{aligned} & 34500307 . \\ & 45 \end{aligned}$ | $\begin{aligned} & 17689735.0 \\ & 4 \end{aligned}$ | $\begin{aligned} & 4988352.9 \\ & 91 \end{aligned}$ |
| F | 47 | $\begin{aligned} & 6354296.5 \\ & 63 \end{aligned}$ | $\begin{aligned} & 70834557 . \\ & 87 \end{aligned}$ | $\begin{aligned} & 42887923 . \\ & 04 \end{aligned}$ | $\begin{aligned} & 36915328 . \\ & 98 \end{aligned}$ | 18928016.5 | 5337537.7 |
|  |  |  |  |  |  |  |  |
|  |  |  |  | Total TTC= | $\begin{aligned} & 250907145 \\ & 3 \end{aligned}$ |  |  |

So total save $=305818457.4$

So for TTC we can say multilane is more preferable where we can save 305818457.4 taka almost.

## Chapter 8

## Vehicle Operating Cost

Vehicle operating cost in Multilane

| Heavy <br> Truck | Medium <br> Truck | Small Truck | Large <br> Bus | Minibus | Microbus | Utility | Car | Auto- <br> Rickshaw | Motorcycle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 199686 | 847970.7 | 338466.9576 | 21514.61 | 183109.6 | 254537.6 | 34542.14 | 454754.982 | 76972.22 | 50916.64 |
| 21366 | 9073 | 362159.6446 | 23020.63 | 195927. | 272355.2 | 36960.09 | 486587.831 | 82360.27 | 54480.8 |
| 228620.5 | 9708 | 387510.819 | 24632.0 | 209642.2 | 291 | 39547.3 | 520648.979 | 88125.49 | 58294.46 |
| 244623.9 | 103880 | 414636.5771 | 26356.32 | 224317.1 | 311819.5 | 42315.61 | 557094.408 | 94294.27 | 62375.07 |
| 261747.6 | 1111517 | 443661.1375 | 28201.26 | 240019.3 | 333646.8 | 45277.7 | 596091.016 | 100894.9 | 66741.32 |
| 280069. | 11893 | 474717.41 | 30175.3 | 256820.7 | 357002. | 48447.14 | 637817.387 | 107957.5 | 71413.22 |
| 299674.8 | 12725 | 507947.636 | 32287.62 | 274798. | 381992.3 | 51838.44 | 682464.605 | 115514.5 | 76412.14 |
| 320652.1 | 1361656 | 543503.9709 | 34547.75 | 294034 | 408731.7 | 55467.13 | 730237.127 | 123600.6 | 81760.99 |
| 343097. | 14569 | 581549.2 | 36966.1 | 31461 | 437343 | 59349.83 | 781353.726 | 132252.6 | 87484.26 |
| 3671 | 155896 | 622257 | 3955 | 336639 | 467 | 63504.31 | 836048.486 | 141510 | 93608.16 |
| 392812.6 | 1668087 | 665815.735 | 42322.48 | 360204.3 | 500713.9 | 67949.62 | 894571.881 | 151416 | 100160.7 |
| 420309.5 | 1784853 | 712422.8365 | 45285.06 | 385418.6 | 535763.9 | 72706.09 | 957191.912 | 162015.1 | 07172 |
| 449731. | 190979 | 762292 | 4845 | 412 | 57326 | 7779 | 1024195.35 | 173356.2 | 114674 |
| 481212.3 | 2043478 | 815652.9055 | 51846.86 | 441265.8 | 613396.1 | 83241.2 | 1095889.02 | 185491.1 | 122701.2 |
| 514897.2 | 2186522 | 872748.6089 | 55476.14 | 472154.4 | 656333.8 | 89068.09 | 1172601.25 | 198475.5 | 131290.3 |
| 550940 | 233957 | 933841.011 | 59359.47 | 505205. | 702277 | 95302.85 | 1254683.34 | 212368.8 | 140480.6 |
| 589505.7 | 2503349 | 999209.8823 | 63514.64 | 540569.5 | 751436.6 | 101974.1 | 1342511.17 | 227234.6 | 150314.2 |
| 630771.2 | 2678583 | 1069154.574 | 67960.66 | 578409.4 | 804037.2 | 109112.2 | 1436486.96 | 243141 | 160836.2 |
| 674925.1 | 2866084 | 1143995.394 | 72717.91 | 618898.1 | 860319.8 | 116750.1 | 1537041.04 | 260160.9 | 172094.8 |
| 722169.9 | 3066710 | 1224075.072 | 77808.16 | 662220.9 | 920542.2 | 124922.6 | 1644633.91 | 278372.1 | 184141.4 |
| 772721.8 | 3281379 | 1309760.327 | 83254.73 | 708576.4 | 984980.1 | 133667.2 | 1759758.29 | 297858.2 | 197031.3 |
| 826812.3 | 3511076 | 1401443.55 | 89082.56 | 758176.7 | 1053929 | 143023.9 | 1882941.37 | 318708.3 | 210823.5 |
| 884689.2 | 3756851 | 1499544.598 | 95318.34 | 811249.1 | 1127704 | 153035.6 | 2014747.27 | 341017.8 | 225581.2 |


| 946617.4 | 4019831 | 1604512.72 | 101990.6 | 868036.5 | 1206643 | 163748 | 2155779.57 | 364889.1 | 241371.8 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1012881 | 4301219 | 1716828.611 | 109130 | 928799.1 | 1291108 | 175210.4 | 2306684.14 | 390431.3 | 258267.9 |
| 1083782 | 4602304 | 1837006.613 | 116769.1 | 993815 | 1381486 | 187475.1 | 2468152.03 | 417761.5 | 276346.6 |
| 1159647 | 4924465 | 1965597.076 | 124942.9 | 1063382 | 1478190 | 200598.4 | 2640922.68 | 447004.8 | 295690.9 |
| 1240822 | 5269178 | 2103188.872 | 133688.9 | 1137819 | 1581663 | 214640.3 | 2825787.26 | 478295.2 | 316389.2 |
| 1327680 | 5638020 | 2250412.093 | 143047.1 | 1217466 | 1692379 | 229665.1 | 3023592.37 | 511775.8 | 338536.5 |
| 1420617 | 6032682 | 2407940.939 | 153060.4 | 1302689 | 1810846 | 245741.7 | 3235243.84 | 547600.1 | 362234 |
| 1520061 | 6454970 | 2576496.805 | 163774.7 | 1393877 | 1937605 | 262943.6 | 3461710.91 | 585932.1 | 387590.4 |
| 1626465 | 6906817 | 2756851.581 | 175238.9 | 1491448 | 2073237 | 281349.6 | 3704030.67 | 626947.4 | 414721.8 |
| 1740318 | 7390295 | 2949831.192 | 187505.6 | 1595850 | 2218364 | 301044.1 | 3963312.82 | 670833.7 | 443752.3 |
| 1862140 | 7907615 | 3156319.375 | 200631 | 1707559 | 2373649 | 322117.2 | 4240744.71 | 717792.1 | 474814.9 |
| 1992490 | 8461148 | 3377261.731 | 214675.2 | 1827088 | 2539805 | 344665.4 | 4537596.84 | 768037.5 | 508052 |
| 2131964 | 9053429 | 3613670.053 | 229702.4 | 1954985 | 2717591 | 368792 | 4855228.62 | 821800.1 | 543615.6 |
| 2281201 | 9687169 | 3866626.956 | 245781.6 | 2091834 | 2907823 | 394607.4 | 5195094.63 | 879326.1 | 581668.7 |
| 2440885 | 10365271 | 4137290.843 | 262986.3 | 2238262 | 3111370 | 422229.9 | 5558751.25 | 940879 | 622385.5 |
| 2611747 | 11090840 | 4426901.202 | 281395.4 | 2394940 | 3329166 | 451786 | 5947863.84 | 1006741 | 665952.5 |
| 2794570 | 11867198 | 4736784.286 | 301093 | 2562586 | 3562208 | 483411 | 6364214.31 | 1077212 | 712569.2 |
| 2990189 | 12697902 | 5068359.187 | 322169.5 | 2741967 | 3811562 | 517249.8 | 6809709.31 | 1152617 | 762449 |
| 3199503 | 13586755 | 5423144.33 | 344721.4 | 2933905 | 4078372 | 553457.3 | 7286388.96 | 1233300 | 815820.5 |
| 3423468 | 14537828 | 5802764.433 | 368851.9 | 3139278 | 4363858 | 592199.3 | 7796436.19 | 1319631 | 872927.9 |
| 3663111 | 15555476 | 6208957.943 | 394671.5 | 3359027 | 4669328 | 633653.3 | 8342186.72 | 1412006 | 934032.8 |
| 3919528 | 16644360 | 6643584.999 | 422298.6 | 3594159 | 4996181 | 678009 | 8926139.79 | 1510846 | 999415.1 |
| 4193895 | 17809465 | 7108635.949 | 451859.5 | 3845751 | 5345913 | 725469.6 | 9550969.58 | 1616605 | 1069374 |
| 4487468 | 19056127 | 7606240.465 | 483489.6 | 4114953 | 5720127 | 776252.5 | 10219537.4 | 1729768 | 1144230 |
|  | Total= | 793942656.3 |  |  |  |  |  |  |  |

VOC in two lane

| $\begin{aligned} & \mathrm{Ye} \\ & \text { ar } \end{aligned}$ | Heavy <br> Truck | Mediu <br> m <br> Truck | Small <br> Truck | Large Bus | Minibu <br> s | Microb us | Utility | Car | Auto- <br> Ricksh <br> aw | Motorcy <br> cle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\begin{array}{r} 20649 \\ 1.7 \end{array}$ | $882823$ $\text { . } 9$ | 351968.1 | $\begin{array}{r} 22512.59 \\ 34 \end{array}$ | $\begin{array}{r} \hline 18861 \\ 8.2 \end{array}$ | $263992$ $.7$ | $36068 .$ $47$ | 463934 .4 | $\begin{array}{r} 78174 . \\ 91 \end{array}$ | $50916.6$ $4$ |
| 2 | $\begin{array}{r} 22094 \\ 6.1 \end{array}$ | $944621$ $\text { . } 6$ | 376605.9 | $\begin{array}{r} 24088.47 \\ 494 \end{array}$ | $\begin{array}{r} 20182 \\ 1.5 \end{array}$ | $282472$ $.2$ | $38593 .$ $27$ | $\begin{array}{r} 496409 \\ .8 \end{array}$ | $83647 .$ | 54480.8 |
| 3 | $\begin{array}{r} 23641 \\ 2.4 \end{array}$ | $101074$ | 402968.3 | $\begin{array}{r} 25774.66 \\ 818 \end{array}$ | $\begin{array}{r} 21594 \\ 9 \end{array}$ | $302245$ $.2$ | $41294 .$ $8$ | $\begin{array}{r} 531158 \\ .5 \end{array}$ | $\begin{array}{r} 89502 . \\ 45 \end{array}$ | $58294.4$ |
| 4 | $\begin{array}{r} 25296 \\ 1.2 \end{array}$ | 108149 7 | 431176.1 | $\begin{array}{r} 27578.89 \\ 496 \end{array}$ | $\begin{array}{r} 23106 \\ 5.4 \end{array}$ | $\begin{array}{r} 323402 \\ \hline .4 \end{array}$ | 44185. 43 | $\begin{array}{r} 568339 \\ .6 \end{array}$ | 95767. 62 | 62375.0 7 |
| 5 | $\begin{array}{r} 27066 \\ 8.5 \end{array}$ | $\begin{array}{r} 115720 \\ 2 \end{array}$ | 461358.4 | $\begin{array}{r} 29509.41 \\ 76 \end{array}$ | $\begin{array}{r} 24724 \\ 0 \end{array}$ | $346040$ | $\begin{array}{r} 47278 . \\ 41 \end{array}$ | $\begin{array}{r} 608123 \\ .4 \end{array}$ | $\begin{array}{r} 102471 \\ .4 \end{array}$ | $66741.3$ $2$ |
| 6 | $\begin{array}{r} 28961 \\ 5.3 \end{array}$ | $123820$ $6$ | 493653.5 | $\begin{array}{r} 31575.07 \\ 684 \end{array}$ | $\begin{array}{r} 26454 \\ 6.8 \end{array}$ | $370263$ <br> .4 | 50587. <br> 9 | 650692 | $109644$ | $\begin{array}{r} 71413.2 \\ 2 \end{array}$ |
| 7 | $\begin{array}{r} \hline 30988 \\ 8.4 \end{array}$ | $132488$ $1$ | 528209.3 | $\begin{array}{r} 33785.33 \\ 221 \end{array}$ | $\begin{array}{r} 28306 \\ 5 \end{array}$ | $396181$ <br> .8 | $\begin{array}{r} 54129 . \\ 05 \end{array}$ | $\begin{array}{r} 696240 \\ .5 \end{array}$ | $117319$ $.5$ | $76412.1$ |
| 8 | $\begin{array}{r} 33158 \\ 0.6 \end{array}$ | $\begin{array}{r} 141762 \\ 2 \end{array}$ | 565183.9 | $\begin{array}{r} 36150.30 \\ 547 \end{array}$ | $\begin{array}{r} 30287 \\ 9.6 \end{array}$ | $423914$ $\text { . } 6$ | $\begin{array}{r} \hline 57918 . \\ 09 \end{array}$ | $\begin{array}{r} 744977 \\ .3 \end{array}$ | $\begin{array}{r} 125531 \\ .8 \end{array}$ | $\begin{array}{r} 81760.9 \\ 9 \end{array}$ |
| 9 | $\begin{array}{r} 35479 \\ 1.2 \end{array}$ | 151685 6 | 604746.8 | $\begin{array}{r} 38680.82 \\ 685 \end{array}$ | $32408$ <br> 1.2 | $453588$ <br> . 6 | $\begin{array}{r} 61972 . \\ 36 \end{array}$ | $\begin{array}{r} 797125 \\ .7 \end{array}$ | 134319 | 87484.2 <br> 6 |
| 10 | $\begin{array}{r} \hline 37962 \\ 6.6 \end{array}$ | $162303$ $6$ | 647079.1 | $\begin{array}{r} 41388.48 \\ 473 \end{array}$ | $\begin{array}{r} 34676 \\ 6.9 \end{array}$ | $485339$ <br> .8 | 66310. 42 | $\begin{array}{r} 852924 \\ .5 \end{array}$ | $143721$ | 93608.1 |
| 11 | $\begin{array}{r} 40620 \\ 0.5 \end{array}$ | $173664$ $8$ | 692374.6 | $\begin{array}{r} 44285.67 \\ 866 \end{array}$ | $\begin{array}{r} 37104 \\ 0.5 \end{array}$ | $\begin{array}{r} 519313 \\ .6 \end{array}$ | $\begin{array}{r} 70952 . \\ 15 \end{array}$ | $\begin{array}{r} 912629 \\ .3 \end{array}$ | $\begin{array}{r} 153781 \\ .9 \end{array}$ | $100160 .$ $7$ |
| 12 | $\begin{array}{r} 43463 \\ 4.5 \end{array}$ | 185821 <br> 4 | 740840.8 | $\begin{array}{r} 47385.67 \\ 617 \end{array}$ | $\begin{array}{r} 39701 \\ 3.4 \end{array}$ | $555665$ | $75918 .$ | $976513$ $.3$ | $164546$ | 107172 |


| 13 | $\begin{array}{r} 46505 \\ 8.9 \end{array}$ | $\begin{array}{r} 198828 \\ 9 \end{array}$ | 792699.7 | $\begin{array}{r} \hline 50702.67 \\ 35 \end{array}$ | $\begin{array}{r} 42480 \\ 4.3 \end{array}$ | $\begin{array}{r} 594562 \\ .1 \end{array}$ | $\begin{array}{r} 81233 . \\ 12 \end{array}$ | $\begin{array}{r} 104486 \\ 9 \end{array}$ | $\begin{array}{r} 176064 \\ .9 \end{array}$ | 114674 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | $\begin{array}{r} 49761 \\ 3 \end{array}$ | $\begin{array}{r} 212746 \\ 9 \end{array}$ | 848188.6 | $\begin{array}{r} \hline 54251.86 \\ 065 \end{array}$ | $\begin{array}{r} 45454 \\ 0.6 \end{array}$ | $\begin{array}{r} 636181 \\ .5 \end{array}$ | 86919. 43 | $\begin{array}{r} 111801 \\ 0 \end{array}$ | $188389$ $.4$ | 122701. <br> 2 |
| 15 | $\begin{array}{r} 53244 \\ 5.9 \end{array}$ | $227639$ $2$ | 907561.8 | $\begin{array}{r} \hline 58049.49 \\ 089 \end{array}$ | $\begin{array}{r} 48635 \\ 8.4 \end{array}$ | $680714$ $.2$ | $\begin{array}{r} 93003 . \\ 79 \end{array}$ | $119627$ $1$ | $201576$ $.7$ | $131290 .$ $3$ |
| 16 | $\begin{array}{r} 56971 \\ 7.1 \end{array}$ | $\begin{array}{r} 243573 \\ 9 \end{array}$ | 971091.2 | $\begin{array}{r} 62112.95 \\ 525 \end{array}$ | $\begin{array}{r} 52040 \\ 3.5 \end{array}$ | $\begin{array}{r} 728364 \\ .2 \end{array}$ | 99514. 06 | $\begin{array}{r} 128001 \\ 0 \end{array}$ | 215687 | $140480 .$ $6$ |
| 17 | $\begin{array}{r} 60959 \\ 7.3 \end{array}$ | $260624$ $1$ | 1039068 | $\begin{array}{r} 66460.86 \\ 212 \end{array}$ | $\begin{array}{r} 55683 \\ 1.8 \end{array}$ | $\begin{array}{r} 779349 \\ .6 \end{array}$ | $\begin{array}{r} 10648 \\ 0 \end{array}$ | $136961$ $0$ | $230785$ | $150314 .$ |
| 18 | $\begin{array}{r} 65226 \\ 9.2 \end{array}$ | $\begin{array}{r} 278867 \\ 8 \end{array}$ | 1111802 | $\begin{array}{r} 71113.12 \\ 247 \end{array}$ | $\begin{array}{r} 59581 \\ 0 \end{array}$ | $\begin{array}{r} 833904 \\ .1 \end{array}$ | $\begin{array}{r} 11393 \\ 3.6 \end{array}$ | $\begin{array}{r} 146548 \\ 3 \end{array}$ | $\begin{array}{r} 246940 \\ .1 \end{array}$ | $160836 .$ |
| 19 | $\begin{array}{r} 69792 \\ 8 \end{array}$ | $298388$ | 1189628 | $\begin{array}{r} \hline 76091.04 \\ 104 \end{array}$ | $\begin{array}{r} 63751 \\ 6.7 \end{array}$ | $892277$ $.4$ | $\begin{array}{r} \hline 12190 \\ 9 \end{array}$ | $156806$ $7$ | $\begin{array}{r} 264225 \\ .9 \end{array}$ | $172094 .$ |
| 20 | $\begin{array}{r} 74678 \\ 3 \end{array}$ | $319275$ $7$ | 1272902 | $\begin{array}{r} 81417.41 \\ 392 \end{array}$ | $\begin{array}{r} 68214 \\ 2.9 \end{array}$ | $\begin{array}{r} 954736 \\ .8 \end{array}$ | $\begin{array}{r} 13044 \\ 2.6 \end{array}$ | $167783$ $2$ | $\begin{array}{r} 282721 \\ .7 \end{array}$ | $184141 .$ $4$ |
| 21 | $\begin{array}{r} 79905 \\ 7.8 \end{array}$ | $\begin{array}{r} 341625 \\ 0 \end{array}$ | 1362006 | $\begin{array}{r} 87116.63 \\ 289 \end{array}$ | $\begin{array}{r} 72989 \\ 2.9 \end{array}$ | $102156$ | $\begin{array}{r} 13957 \\ 3.6 \end{array}$ | $\begin{array}{r} 179528 \\ 0 \end{array}$ | $302512$ $.2$ | $197031 .$ $3$ |
| 22 | $\begin{array}{r} 85499 \\ 1.8 \end{array}$ | $365538$ <br> 8 | 1457346 | $\begin{array}{r} \hline 93214.79 \\ 719 \end{array}$ | $78098$ <br> 5.4 | $109307$ $8$ | $\begin{array}{r} 14934 \\ 3.8 \end{array}$ | $192094$ $9$ | $\begin{array}{r} 323688 \\ .1 \end{array}$ | $210823 .$ |
| 23 | $91484$ <br> 1.2 | $\begin{array}{r} 391126 \\ 5 \end{array}$ | 1559360 | $\begin{array}{r} 99739.83 \\ 3 \end{array}$ | 83565 <br> 4.4 | $\begin{array}{r} 116959 \\ 4 \end{array}$ | $\begin{array}{r} 15979 \\ 7.8 \end{array}$ | $\begin{array}{r} 205541 \\ 6 \end{array}$ | $\begin{array}{r} 346346 \\ .2 \end{array}$ | $225581 .$ $2$ |
| 24 | $\begin{array}{r} 97888 \\ 0.1 \end{array}$ | $\begin{array}{r} 418505 \\ 3 \end{array}$ | 1668515 | $\begin{array}{r} 106721.6 \\ 213 \end{array}$ | $\begin{array}{r} 89415 \\ 0.2 \end{array}$ | $\begin{array}{r} 125146 \\ 5 \end{array}$ | $\begin{array}{r} 17098 \\ 3.7 \end{array}$ | $\begin{array}{r} 219929 \\ 5 \end{array}$ | $\begin{array}{r} 370590 \\ .5 \end{array}$ | $241371 .$ $8$ |
| 25 | $\begin{array}{r} 10474 \\ 02 \end{array}$ | $\begin{array}{r} 447800 \\ 7 \end{array}$ | 1785312 | $\begin{array}{r} 114192.1 \\ 348 \end{array}$ | $\begin{array}{r} 95674 \\ 0.7 \end{array}$ | $\begin{array}{r} 133906 \\ 8 \end{array}$ | $\begin{array}{r} 18295 \\ 2.5 \end{array}$ | $235324$ $6$ | $\begin{array}{r} 396531 \\ .8 \end{array}$ | $258267$ <br> 9 |
| 26 | $\begin{array}{r} 11207 \\ 20 \end{array}$ | $\begin{array}{r} 479146 \\ 7 \end{array}$ | 1910283 | $\begin{array}{r} 122185.5 \\ 842 \end{array}$ | $\begin{array}{r} 10237 \\ 13 \end{array}$ | $\begin{array}{r} 143280 \\ 3 \end{array}$ | $\begin{array}{r} 19575 \\ 9.2 \end{array}$ | $\begin{array}{r} 251797 \\ 3 \end{array}$ | 424289 | $276346 .$ |
| 27 | $\begin{array}{r} 11991 \\ 70 \end{array}$ | $\begin{array}{r} 512687 \\ 0 \end{array}$ | 2044003 | $\begin{array}{r} 130738.5 \\ 751 \end{array}$ | $\begin{array}{r} 10953 \\ 72 \end{array}$ | $\begin{array}{r} 153309 \\ 9 \end{array}$ | $\begin{array}{r} 20946 \\ 2.4 \end{array}$ | $\begin{array}{r} 269423 \\ 1 \end{array}$ | $\begin{array}{r} \hline 453989 \\ .3 \end{array}$ | $\begin{array}{r} 295690 . \\ 9 \end{array}$ |


| 28 | $\begin{array}{r} 12831 \\ 12 \end{array}$ | $\begin{array}{r} 548575 \\ 1 \end{array}$ | 2187083 | $\begin{array}{r} 139890.2 \\ 754 \end{array}$ | $\begin{array}{r} 11720 \\ 48 \end{array}$ | $\begin{array}{r} 164041 \\ 6 \end{array}$ | $\begin{array}{r} 22412 \\ 4.7 \end{array}$ | $\begin{array}{r} 288282 \\ 7 \end{array}$ | $\begin{array}{r} 485768 \\ .5 \end{array}$ | 316389. <br> 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29 | $\begin{array}{r} 13729 \\ 30 \end{array}$ | $586975$ | 2340179 | $\begin{array}{r} 149682.5 \\ 947 \end{array}$ | $\begin{array}{r} 12540 \\ 92 \end{array}$ | $\begin{array}{r} 175524 \\ 5 \end{array}$ | $\begin{array}{r} 23981 \\ 3.5 \end{array}$ | $\begin{array}{r} 308462 \\ 5 \end{array}$ | $\begin{array}{r} \hline 519772 \\ .3 \end{array}$ | $\begin{array}{r} 338536 . \\ 5 \end{array}$ |
| 30 | $\begin{array}{r} 14690 \\ 35 \end{array}$ | $\begin{array}{r} 628063 \\ 6 \end{array}$ | 2503992 | $\begin{array}{r} 160160.3 \\ 763 \end{array}$ | $\begin{array}{r} 13418 \\ 78 \end{array}$ | $\begin{array}{r} 187811 \\ 2 \end{array}$ | $\begin{array}{r} 25660 \\ 0.4 \end{array}$ | $\begin{array}{r} 330054 \\ 9 \end{array}$ | $\begin{array}{r} 556156 \\ .4 \end{array}$ | 362234 |
| 31 | $\begin{array}{r} 15718 \\ 68 \end{array}$ | $\begin{array}{r} 672028 \\ 1 \end{array}$ | 2679271 | $\begin{array}{r} 171371.6 \\ 026 \end{array}$ | $\begin{array}{r} 14358 \\ 10 \end{array}$ | $\begin{array}{r} 200958 \\ 0 \end{array}$ | $\begin{array}{r} 27456 \\ 2.4 \end{array}$ | $\begin{array}{r} 353158 \\ 7 \end{array}$ | $595087$ | $387590 .$ <br> 4 |
| 32 | 16818 98 | $\begin{array}{r} 719070 \\ 1 \end{array}$ | 2866820 | $183367.6$ $148$ | $15363$ $16$ | $\begin{array}{r} 215025 \\ 0 \end{array}$ | $29378$ <br> 1.8 | $\begin{array}{r} 377879 \\ 8 \end{array}$ | $636743$ | $414721 .$ |
| 33 | $\begin{array}{r} 17996 \\ 31 \end{array}$ | $\begin{array}{r} 769405 \\ 0 \end{array}$ | 3067498 | $\begin{array}{r} 196203.3 \\ 479 \end{array}$ | 16438 <br> 59 | $\begin{array}{r} 230076 \\ 8 \end{array}$ | $\begin{array}{r} 31434 \\ 6.5 \end{array}$ | $404331$ $4$ | $\begin{array}{r} 681315 \\ .5 \end{array}$ | $443752 .$ |
| 34 | $\begin{array}{r} 19256 \\ 05 \end{array}$ | $\begin{array}{r} 823263 \\ 3 \end{array}$ | 3282222 | $\begin{array}{r} 209937.5 \\ 822 \end{array}$ | $\begin{array}{r} 17589 \\ 29 \end{array}$ | $\begin{array}{r} 246182 \\ 2 \end{array}$ | $\begin{array}{r} 33635 \\ 0.8 \end{array}$ | $432634$ $6$ | $\begin{array}{r} 729007 \\ .6 \end{array}$ | $474814 .$ |
| 35 | $\begin{array}{r} 20603 \\ 98 \end{array}$ | $880891$ | 3511978 | $224633.2$ $13$ | $\begin{array}{r} 18820 \\ 54 \end{array}$ | $263414$ | $35989$ $5.3$ | $462919$ | $\begin{array}{r} 780038 \\ .1 \end{array}$ | 508052 |
| 36 | $\begin{array}{r} 22046 \\ 26 \end{array}$ | $942554$ $2$ | 3757816 | $\begin{array}{r} \hline 240357.5 \\ 379 \end{array}$ | 20137 <br> 97 | $\begin{array}{r} 281853 \\ 9 \end{array}$ | $\begin{array}{r} 38508 \\ 8 \end{array}$ | $495323$ $4$ | $\begin{array}{r} 834640 \\ .8 \end{array}$ | 543615. <br> 6 |
| 37 | 23589 <br> 49 | 100853 | 4020864 | $\begin{array}{r} \hline 257182.5 \\ 655 \end{array}$ | $21547$ $63$ | $\begin{array}{r} 301583 \\ 7 \end{array}$ | $\begin{array}{r} 41204 \\ 4.2 \end{array}$ | $\begin{array}{r} 529996 \\ 0 \end{array}$ | 893065 <br> . 6 | 581668. <br> 7 |
| 38 | $\begin{array}{r} 25240 \\ 76 \end{array}$ | $\begin{array}{r} 107913 \\ 03 \end{array}$ | 4302324 | $\begin{array}{r} 275185.3 \\ 451 \end{array}$ | $\begin{array}{r} 23055 \\ 97 \end{array}$ | $\begin{array}{r} 322694 \\ 6 \end{array}$ | $44088$ $7.3$ | $567095$ $7$ | $\begin{array}{r} 955580 \\ .2 \end{array}$ | $622385 .$ |
| 39 | $\begin{array}{r} 27007 \\ 61 \end{array}$ | $\begin{array}{r} 115466 \\ 94 \end{array}$ | 4603487 | $\begin{array}{r} 294448.3 \\ 193 \end{array}$ | 24669 89 | $\begin{array}{r} 345283 \\ 2 \end{array}$ | $\begin{array}{r} 47174 \\ 9.4 \end{array}$ | $606792$ $4$ | $102247$ $1$ | $665952 .$ |
| 40 | $\begin{array}{r} 28898 \\ 14 \end{array}$ | $\begin{array}{r} 123549 \\ 63 \end{array}$ | 4925731 | $\begin{array}{r} 315059.7 \\ 016 \end{array}$ | $\begin{array}{r} 26396 \\ 78 \end{array}$ | $369453$ $0$ | $\begin{array}{r} 50477 \\ 1.8 \end{array}$ | $649267$ | $109404$ $4$ | $712569 .$ |
| 41 | $\begin{array}{r} 30921 \\ 01 \end{array}$ | $132198$ $10$ | 5270532 | $\begin{array}{r} 337113.8 \\ 807 \end{array}$ | $28244$ | $395314$ $7$ | $\begin{array}{r} 54010 \\ 5.9 \end{array}$ | $694716$ $7$ | $117062$ $7$ | 762449 |
| 42 | 33085 <br> 49 | $141451$ $97$ | 5639469 | $\begin{array}{r} 360711.8 \\ 524 \end{array}$ | 30221 67 | $\begin{array}{r} 422986 \\ 8 \end{array}$ | $\begin{array}{r} 57791 \\ 3.3 \end{array}$ | $\begin{array}{r} \hline 743346 \\ 8 \end{array}$ | $125257$ $1$ | $815820 .$ |


|  | 35401 | 151353 |  | 385961.6 | 32337 | 452595 | 61836 | 795381 | 134025 | 872927. |
| ---: | ---: | ---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 43 | 47 | 60 | 6034232 | 82 | 19 | 8 | 7.2 | 1 | 1 | 9 |
| 44 | 37879 | 161948 |  | 412978.9 | 34600 | 484277 | 66165 | 851057 | 143406 | 934032. |
|  | 57 | 36 | 6456628 | 998 | 79 | 6 | 2.9 | 8 | 8 | 8 |
| 45 | 40531 | 173284 |  | 441887.5 | 37022 | 518177 | 70796 | 910631 | 153445 | 999415. |
|  | 14 | 74 | 6908592 | 298 | 85 | 0 | 8.6 | 8 | 3 | 1 |
| 46 | 43368 | 185414 |  | 472819.6 | 39614 | 554449 | 75752 | 974376 | 164186 |  |
|  | 32 | 67 | 7392194 | 568 | 44 | 4 | 6.4 | 1 | 5 | 1069374 |
| 47 | 46404 | 198393 |  | 505917.0 | 42387 | 593260 | 81055 | 104258 | 175679 |  |
| 10 | 70 | 7909647 | 328 | 46 | 8 | 3.3 | 24 | 5 | 1144230 |  |

Vehicle Operating cost reduce: 44098582.3

## Chapter 9

## Benefit cost ratio

For flexible pavement:

| Accident Benefit | 1298207516.20 |
| :--- | :--- |
|  |  |
| VOC | 146909646.6 |
| TTC | 305818457.4 |
| Fuel Benefit | 8567542.15 |
| Noise Benefit | 487373484.1 |
| Total Benefit | 2246876646.46 |
|  |  |
| Cost | 131848319.6 |
| Earth Fill | 45203004 |
| Maintenance | 301770095.6 |
| Total Cost | 4.698821419 .2 |
| B/C ratio |  |

In previos discussion we have calculated accident benefit, VOC, TOC, fuel benefit, noice benefit. So our total benefit was 2246876646.46 . afterthan we calculated cost part. Cost was total 478821419.2. we got benefit cost ratio 4.692514905 .

For rigid pavement:

| Accident Benefit | 1298207516.20 |
| :--- | :--- |
| VOC | 146909646.6 |
| TTC | 305818457.4 |
| Fuel Benefit | 8567542.15 |
| Noise Benefit | 487373484.1 |
| Total Benefit | 2246876646.46 |
| Cost | 322644265.9 |


| Earth Fill | 45203004 |
| :--- | :--- |
| Total Cost | 367847269.9 |
| B/C ratio | 6.108178122 |


| Accident Benefit | 1298207516.20 |
| :--- | :--- |
| VOC | 146909646.6 |
| TTC | 305818457.4 |
| Fuel Benefit | 8567542.15 |
| Noise Benefit | 487373484.1 |
| Total Benefit | 2246876646.46 |
| Cost | 288956949.2 |
| Earth Fill | 45203004 |
| Total Cost | 334159953.2 |
| B/C ratio | 6.723955475 |

For first method of rigid pavement we have got benefit cost ratio 6.108178122

And for second method we have got 6.723955475 .
Since the second ratio is higher. So we will choose this one.

So our selected road thickness is 8.5 inches.

## Chapter 10

## Decision on the Pavement

There were three options to make the final decision. The first one was to do nothing, the second one was to choose rigid pavement, and the final option was to choose the flexible pavement.

First of all, doing nothing will not be feasible at all. The level of service will become F within 20 years. The user cost, safety cost, and environmental cost will keep rising up as the level of service got decrease. So, doing nothing was not a viable option.

So, the option remained to choose between rigid pavement and flexible pavement. To choose between these two, weightages were set. The weightages considered were:

| Cost/Benefit | Weightage |
| :--- | :--- |
| Construction and Maintenance Cost | 4 |
| Environmental Benefit | 3 |
| User Benefit | 2 |
| Safety Benefit | 3 |

The weightage of construction and maintenance were the highest. This was considered as saving money is extremely important in todays condition. The rate of dollar is high, the heavy constructions like Padma bridge had already reduced the fund available to the government. Apart from these, many other construction work was ongoing like Metro rail. So, having a lower construction cost was extremely important.

The second highest weightage was set to environmental benefit and safety benefit. These criteria cannot be overlooked. The safety is always the first priority. Accident cost falls under it. In terms of environmental benefit, it was high time environmental benefit of Dhaka city should be taken into consideration. So, these two got the weightage as 3 .

User benefit is important in the long run. However, the other benefits were considered as more important than this one. So, the user benefit got a weightage of 2 .

Table: Rigid Pavement $\mathrm{D}=8.5$ in

| Cost/Benefit Type | Cost/Benefit in BDT | Weightage Type | Weightage | Weighted <br> Amount in BDT |
| :---: | :---: | :---: | :---: | :---: |
| Accident Benefit | 1298207516.20 | Safety | 3 | 3894622549 |
| VOC | 146909646.6 | User <br> Cost/Benefit | 2 | 293819293.2 |
| TTC | 305818457.4 |  |  | 611636914.7 |
| Fuel Benefit | 8567542.15 | Environmental <br> Cost/Benefit | 3 | 25702626.45 |
| Noise Benefit | 487373484.1 |  |  | 1462120452 |
| Total Benefit | 2246876646.46 |  |  | 6287901835 |
| Cost | 288956949.2 | Construction and Maintenance Cost |  | 1155827797 |
| Earth Fill | 45203004 |  | 4 | 180812016 |
| Total Cost | 334159953.2 |  |  | 1336639813 |
| B/C ratio |  |  |  | 4.704260472 |

Table: Flexible Pavement

| Cost/Benefit Type | Cost/Benefit in BDT | Weightage Type | Weightage | Weighted <br> Amount in BDT |
| :---: | :---: | :---: | :---: | :---: |
| Accident Benefit | 1298207516.20 | Safety | 3 | 3894622549 |
| VOC | 146909646.6 | User <br> Cost/Benefit | 2 | 293819293.2 |
| TTC | 305818457.4 |  |  | 611636914.7 |
| Fuel Benefit | 8567542.15 | Environmental Cost/Benefit | 3 | 25702626.45 |
| Noise Benefit | 487373484.1 |  |  | 1462120452 |
| Total Benefit | 2246876646.46 |  |  | 6287901835.42 |
| Cost | 131848319.6 | Construction and Maintenance Cost | 4 | 527393278.3 |
| Earth Fill | 45203004 |  |  | 180812016 |
| Maintenance | 301770095.6 |  |  | 1207080382 |


| Total Cost | 478821419.2 |  |  | 1915285677 |
| :--- | :--- | :--- | :--- | :--- |
| B/C ratio |  | 3.283009899 |  |  |
|  |  |  |  |  |

With the defined weightage, it could be noted that Rigid pavement was more beneficial than the rigid pavement. So, rigid pavement with thickness 8.5 in was decided for this study.

## Project Timeline:



## Project Timeline:

There will be two different works. One is filling earth on the embankment, the other is constructing the pavement. However, before filling the embankment, it will be difficult to construct the pavement as most of the pavement will be built over the filled embankment. So, the 5 tasks are fill, compaction, rebar placement, concrete casting, and curing. None of the work can start before the other gets done.

Total project duration will be 68 days. Among them, all the works have been tentatively set for 8 -10 days. The total length of the road is 8.508 km . So, 1 km each day was the idea to make this project timeline.

Feasibility Study Timeline:


Mode of financing with source: (BDT)

| Mode | Gob(FE) | PA (RPA) | Own Fund | Others | PA source |
| :--- | :---: | ---: | :--- | :--- | :--- |
| Loan/Credit | 0 | 0 | 0 | 0 | 0 |
| Grant | 778821419.2 | 0 | 0 | 0 | 0 |
| Equity | 0 | 0 | 0 | 0 | 0 |
| Others | 0 | 0 | 0 | 0 | 0 |
| Total | 778821419.2 | 0 | 0 | 0 | 0 |

## Chapter 11

## Ethics

To continue a project perfectly and in diciplened way ethics is a topic that should obey by all mandatorily. From the very beginning of a project to the finishing ethical issues come.

Some issues that cannot be excluded when the topic ethics comes in are quality of work, the tender process, accountability of expense, corruption, etc.

First ethical issue occurred in tendering . tendering is the first process of any project. Tender is the process of any entity inviting suppliers to provide a formal written submission for goods or services. By this process entity can select a contractor for construction work on the basis of best value for money. Since entity select a contractor in this process, entity face a lot of difficulty here. Like he can be threated. Many of the times threat come from political involved persons, even law enforcement agencies can not do anything here. Sometimes it happens that tender selection committee member get influenced by money of a candidate and wrong person get choose which is a serious ethical issue for a contraction site.

Then it comes substandard quality of construction work. A well organized construction site build with well educated workers, errorless perfect number of machines, workers with perfect safety tools, well graded construction material. If any of these get short then it is called substandard quality of contraction work. After getting choose in tendering process it is up to contractor to manage all of these. But sometimes it seen that to theft money he do not ensure all standard needs. It is seen that he use less educated, less experienced worker at working site to theft money. Even he use low quality construction material. This is an serious ethical issue to continue perfectly a construction site perfectly.

In a contraction site it is mandatory to obey all safety measures. Firstly a contractor has to manage all safety tools for his workers and he has to ensure that all workers are using those all all time at working time. Then they have to be the most aware of contraction tools that no one of
civil people get hurt. If possible it is high recommended to manage fence around the construction site so that none of a civil people can come in the area. Even security has to be hired for this.

From the contractor to the workers it is most important that they get their money in time. Everyone here do their work for money so that they can manage their life. So it very ethical to give their money in time.

In a project the most threating part is corruption. Corruption is a topic you will see from the very starting of a project to the finish. As we spoke earlier, tender selection committee choose wrong tenderer for money. After that contractor do rest of the damage as we have mentioned earlier. Most of the time we have seen that they give low quality product and less in number. They theft a lot of money from their. Engineers get involved here for money. Sometimes it is seen that contractor, engineer gang use bamboo stick rather than reinforcement. Which is a very serious ethical issue. We see they use low quality and less quantity cement which is suicidal decision. It is sure that accident will occur and we can see lots of accidents in road for road quality. Corruption is a serious ethical issue for a construction side.

Construction project like constructing a road or any big project it is important that everyone become honest and they have to be accountable. In the government project mass people are the main source of investment. So it is responsibility for all the members who are connected with the work to manage media, mass people with proper ethics.

To over overcome all these issues ethics should be taught mandatorily. Everyone related to the project have to know the codes of ethics. Government personnel, tenderer, contractor, workers everyone have to know about the codes of ethics. After then if any one disobey any rule then law enforcement agencies have to be very strict against it.

## Chapter 12

## Cross Section of the Selected Pavement

Base Course 8

## Chapter 13

## BOQ

## Construction Cost for Rigid Pavement:

\(\left.$$
\begin{array}{|l|l|l|l|l|}\hline \text { Description } & \text { Unit } & \text { Quantity } & \text { Rate in BDT } & \begin{array}{l}\text { Amount in } \\
\text { BDT }\end{array} \\
\hline \begin{array}{l}\text { ROAD WAY AND } \\
\text { BORROW } \\
\text { EXCAVATION }\end{array} & & & & \\
\hline \begin{array}{l}\text { Capping Layer compacted } \\
\text { to 95\% MDD,AASHTO } \\
\text { T-180 }\end{array}
$$ \& \& \& \& <br>

\hline SUBBASE \& \& 19,966.40\end{array}\right] 205.2359\)| 4097822.1 |
| :--- |
| Gravel Sub-base <br> layer,97\%MDD,AASHTO <br> T-180 |
| m 3 |


| Longitudinal joints <br> complete (except tie bars | m |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Sealed transverse <br> contraction joints as per <br> the drawing (except <br> Dowels) |  |  | 42.8789 | 425946.13 |
| Dowel bars (mild steel <br> plain bars, epoxy coated) <br> $(25$ mm diameter and 400 <br> mm long at 300 mm <br> spacing): | m | $2,779.40$ | 48.4537 | 134672.21 |
| Tie Bars (Ø 12 mm high <br> strength deformed bars <br> , 1000 mm long @ 600mm <br> spacing, with 15cm long <br> protective coating as per <br> the drawing) | no |  | $9,565.40$ | 145.9403 |


| OR MC-30 prime coat material to be used in the absence of impermeable plastic sheeting, application rate of 1.25lit/m2 | lit | 87,414.84 | 72.5629 | 6343074.3 |
| :---: | :---: | :---: | :---: | :---: |
| Rigid Pavement Total |  |  |  | 250408992 |
| Grand total of the bills without contingency |  |  |  | 255054756 |
| Add 10\% for contingency |  |  |  | 25505476 |
| Add 15\% VAT |  |  |  | 42084035 |
| Total contract amount (including VAT) |  |  |  | 322644266 |

## Construction Cost for Flexible Pavement:

| Description | Unit | Quantity | Rate | Amount in BDT |
| :--- | :--- | :--- | :--- | :--- |
| 5000 SUBBASE, <br> ROAD BASE <br> AND GRAVEL <br> WEARING <br> COURSE |  |  |  |  |
| 5100: SUB- <br> BASES |  |  |  |  |
| Sub-base layer <br> constructed from <br> gravel or Crushed <br> stone: |  |  |  |  |
| a) Gravel sub-base <br> (unstabilized <br> gravel) compacted |  | $7,377.00$ |  | 333.221 |
| to: |  |  |  |  |$\quad$


| Base layer construction a) Gravel base taken from cut or borrow, Gravel base (unstabilized gravel) compacted to: | m 3 | 29,239.00 | 725.9548 | 21226192 |
| :---: | :---: | :---: | :---: | :---: |
| (i) $95 \%$ of modified AASHTO density |  |  |  |  |
| 6000 <br> BITUMINOUS SURFACINGS <br> AND ROAD BASES |  |  |  |  |
| 6100 <br> BITUMINOUS <br> PRIME COAT |  |  |  |  |
| Prime coat |  |  |  |  |
| (a) MC-30 <br> cutback bitumen | Lt | 40,955.90 | 72.5629 | 2971878.9 |
| Tack Coat |  |  |  |  |
| RC -70 Cut back bitumenapplied at 1lit per sq.m | Lt | 205,852.51 | 69.1239 | 14229328 |
| 6300C: DOUBLE <br> SURFACE <br> TREATMENTS |  |  |  |  |
| Double surface treatment using |  |  |  |  |
| (c) Double surface treatment using 20 | m 2 | 80,882.68 | 198.6113 | 16064214 |


| mm and 10 mm <br> chippings (with <br> MC 3000 cutback) |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Variations in the <br> rate of application <br> of Bituminous <br> Binder,with MC <br> 3000 cutback | Lt |  |  |  |
| (h) MC 3000 <br> cutback bitumen | Lt |  |  |  |
| Variations in the <br> rate of application <br> of Chippings |  | $5,877.00$ | 85.7578 |  |
| (a) 20 mm <br> chippings | m 3 |  |  |  |


| Total | 131848320 |
| :--- | :--- |

## Routine Maintenance Cost for Pavements:

Flexible pavement needs to be maintained time to time. If not, the surface may get deteriorated. Once that occurs, the level of service worsen in very short period of time.

Table 3.6: Agency Cost of Flexible pavement

| S/No | Activity | Cost (ETB) | Remarks |
| :---: | :--- | :---: | :--- |
| 1 | Construction Cost | $6,301,638.47$ |  |
| 2 | Routine Maintenance <br> Cost | $673,176.26$ | Twice every <br> year |
| 3 | Periodic Maintenance <br> Cost | $681,856.38$ | Once every <br> three years |
| 4 | Rehabilitation Cost | $2,558,500.84$ | At $15^{\text {th }}$ and $30^{\text {th }}$ <br> years |
| 5 | Salvage Value | $1,705,667.23$ | After $40^{\text {th }}$ years |

Yonus et al. (2016) provided this table for the estimated time period for flexible pavement maintenance. Based on this table, a tentative maintenance schedule and related cost was calculated. The rehabilitation cost has been modified as this projects life cycle is 33 years.

Table:

| Year | Routine cost | Periodic Cost | Rehabilitation <br> Cost | Reconstruction <br> Cost |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1361280 |  |  |  |
| 2 | 1361280 |  |  |  |
| 3 | 1361280 | 4202952 |  |  |
| 4 | 1361280 |  |  |  |
| 5 | 1361280 |  |  |  |
| 6 | 1361280 | 4202952 |  |  |


| 7 | 1361280 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 8 | 1361280 |  |  |  |
| 9 | 1361280 | 4202952 |  |  |
| 10 | 1361280 |  |  |  |
| 11 | 1361280 |  |  |  |
| 12 | 1361280 | 4202952 |  |  |
| 13 | 1361280 |  |  |  |
| 14 | 1361280 |  |  |  |
| 15 | 1361280 | 4202952 | 39383532 |  |
| 16 | 1361280 |  |  |  |
| 17 | 1361280 |  |  |  |
| 18 | 1361280 | 4202952 |  |  |
| 19 | 1361280 |  |  |  |
| 20 | 1361280 |  |  |  |
| 21 | 1361280 | 4202952 |  |  |
| 22 | 1361280 |  |  |  |
| 23 | 1361280 |  |  |  |
| 24 | 1361280 | 4202952 |  |  |
| 25 | 1361280 |  | 39383532 |  |
| 26 | 1361280 |  |  |  |
| 27 | 1361280 | 4202952 |  |  |
| 28 | 1361280 |  |  |  |
| 29 | 1361280 |  |  |  |
| 30 | 1361280 | 4202952 |  |  |
| 31 | 1361280 |  |  |  |
| 32 | 1361280 |  |  |  |
| 33 | 1361280 | 4202952 |  | 49907928 |
| Total | 219829704 |  |  |  |

The total cost for maintenance, rehabilitation, and reconstruction was found to be 219829704 bdt.

In terms of rigid pavement, it does not require any maintenance cost. Once the construction of rigid pavement is completed, it does not require any major maintenance. Thus, the pavement is known as "Fit and Forget".

## Chapter 14

## Legal Issue and Water Resource

Many project report published by the JICA, ADB, and RHD mentioned that the right of way is already owned by the government. On the R112 road, all of the houses, shops, mosque, etc. were built leaving the right of way. So, implementing this project will not produce any legal issue or settlement cost.


As shown in the picture, there are 17.5 m distance left before the water body starts. The road will be only 7.3 m . Those embankments will be filled with soil and a retaining wall will be built before the waterbody. So, the waterbody will remain unchanged.

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